

ECE 342

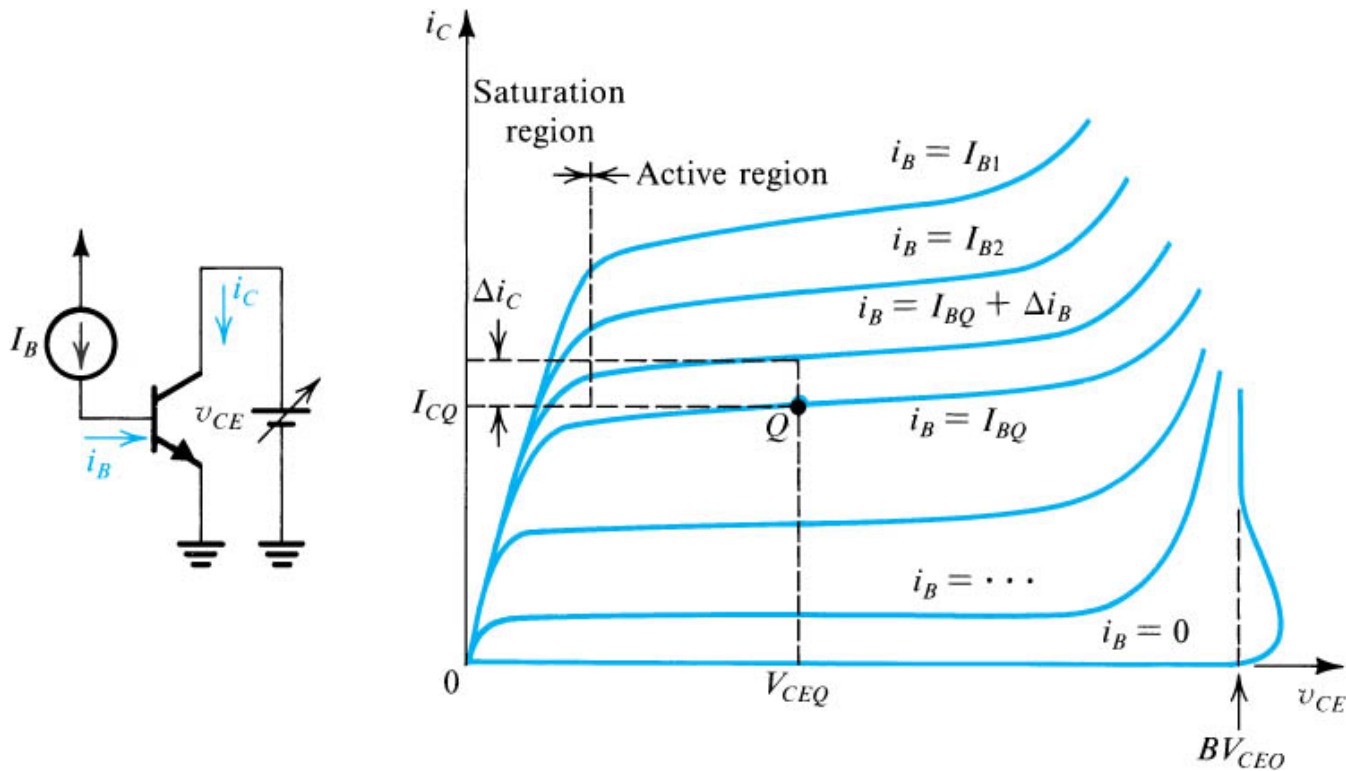
Electronic Circuits

Lecture 15

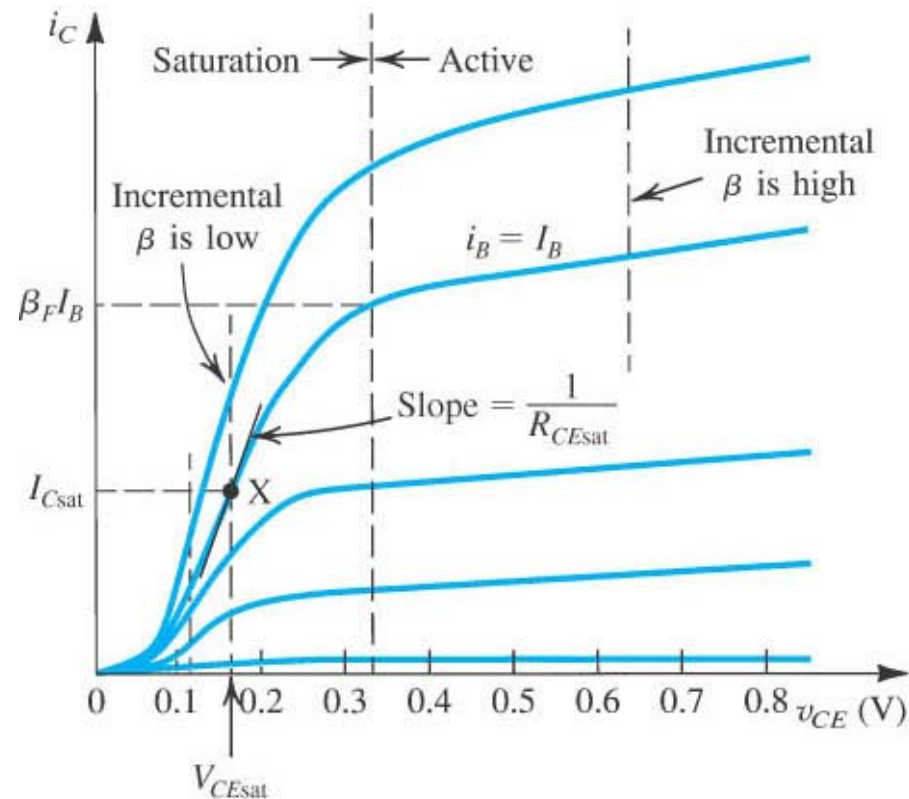
BJT – DC Operation

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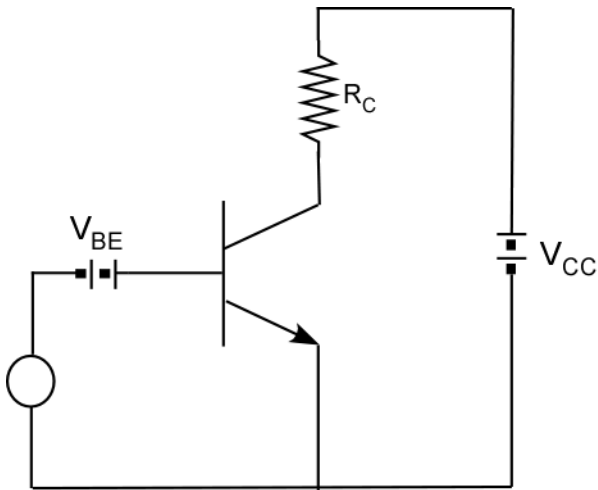
BJT – Common-Emitter Characteristics



BJT – Voltage-Current Characteristics



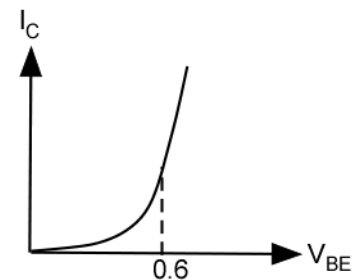
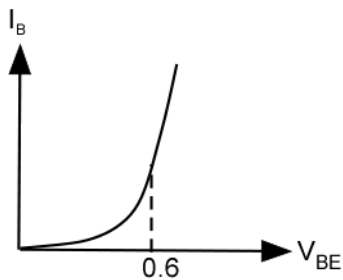
Common Emitter Configuration



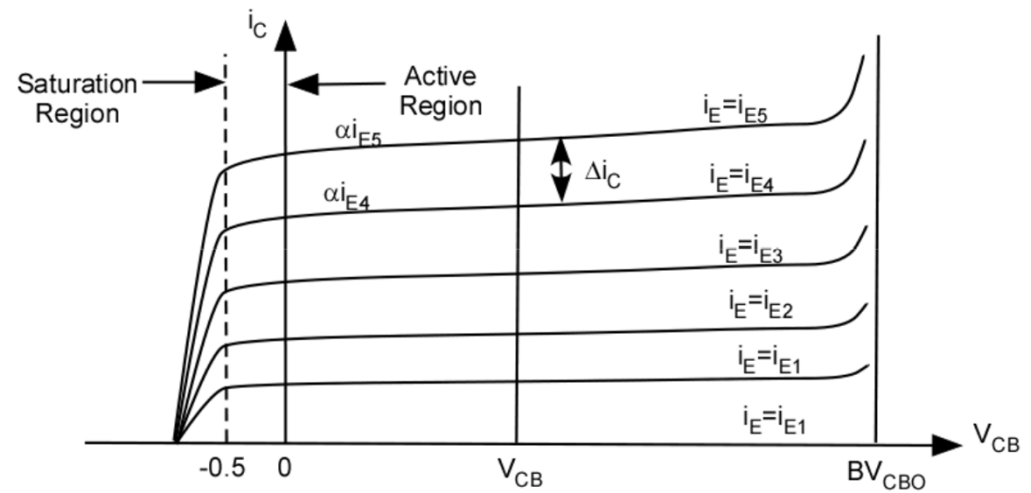
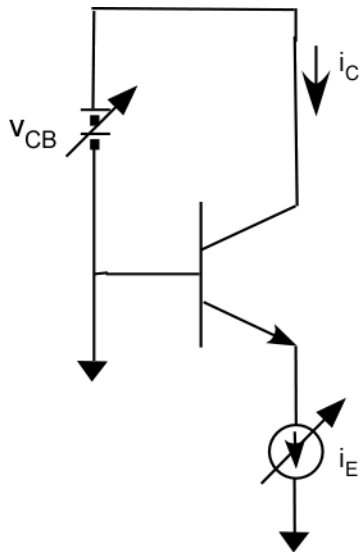
$$I_E = I_B + I_C$$

$$I_C = \alpha I_E$$

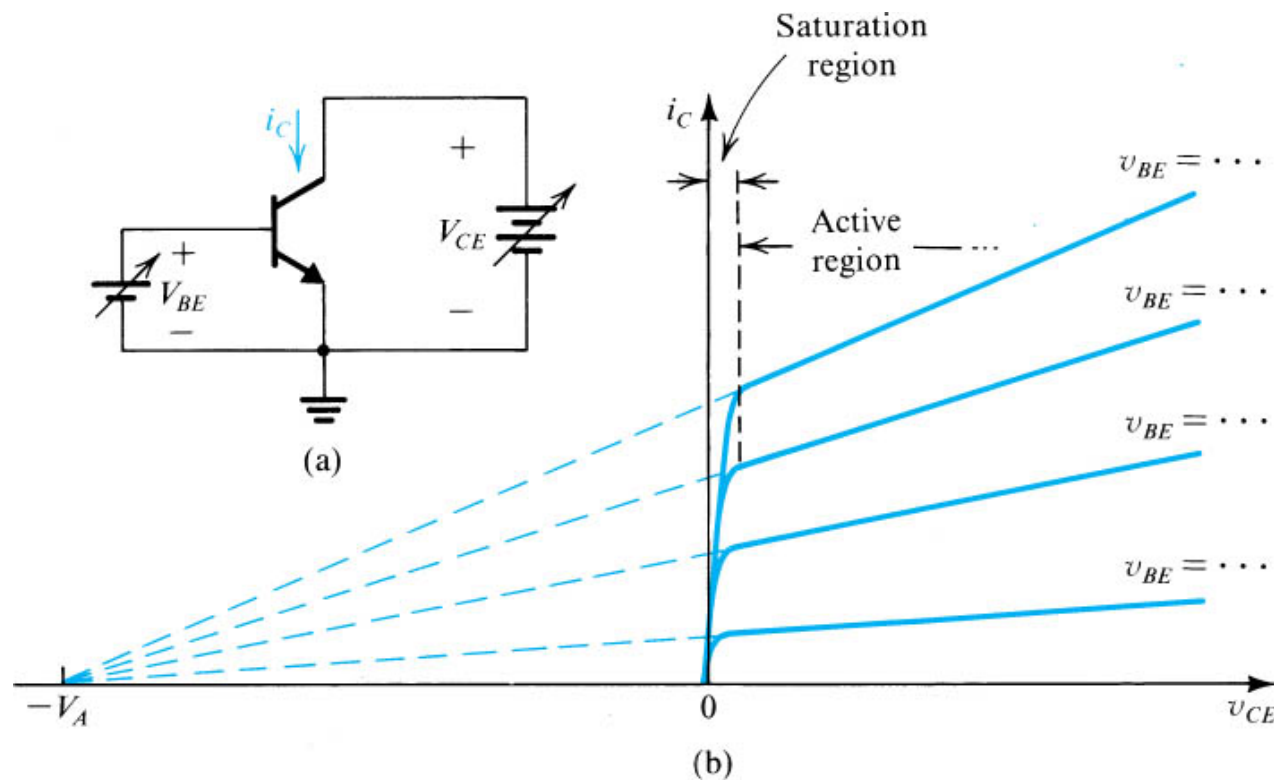
$$I_C = \frac{\alpha}{1 - \alpha} I_B = \beta I_B$$



Common Emitter I-V Characteristics



Early Voltage



- **Early Voltage V_A**
 - Dependence of collector current on collector voltage
 - Increasing V_{CE} increases the width of the depletion region

Output Resistance

r_o is output resistance seen from collector terminal

$$i_C = I_S e^{v_{BE}/V_T} \left(1 + \frac{v_{CE}}{V_A} \right)$$

$$r_o = \left[\frac{\partial i_C}{\partial v_{CE}} \Big|_{v_{BE} = \text{constant}} \right]^{-1}$$

$$r_o = \frac{V_A + V_{CE}}{I_C}$$

Alternatively, neglecting the Early effect on the collector current, we define

$$I'_C = I_S e^{v_{BE}/V_T}$$

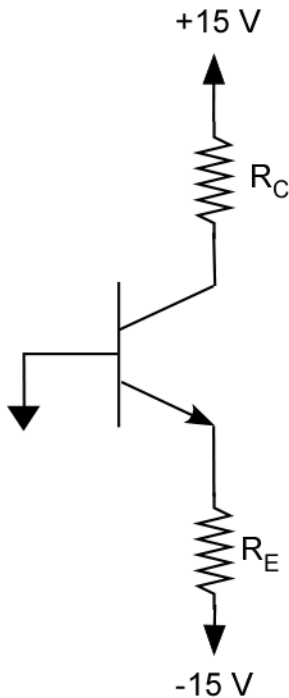
The output resistance then becomes

$$r_o = \frac{V_A}{I'_C}$$

Problem

A transistor has $\beta = 100$, $v_{BE} = 0.7V$ with $I_C = 1$ mA. Design a circuit such that a current of 2 mA flows through the collector and a voltage of 5V appears at the collector.

CBJ reversed biased \rightarrow FAR



Voltage drop across $R_C = 15 - 5 = 10V$

$I_C = 2\text{mA} \rightarrow R_C = 10V / 2\text{mA} = 5\text{k}\Omega$

Since $v_{BE} = 0.7V$ at $I_C = 1$ mA

$$v_{BE} = 0.7 + V_T \ln\left(\frac{2}{1}\right) = 0.717 \text{ V at } 2 \text{ mA}$$

Since base is at 0V, emitter voltage is at -0.717 volts $= V_E$

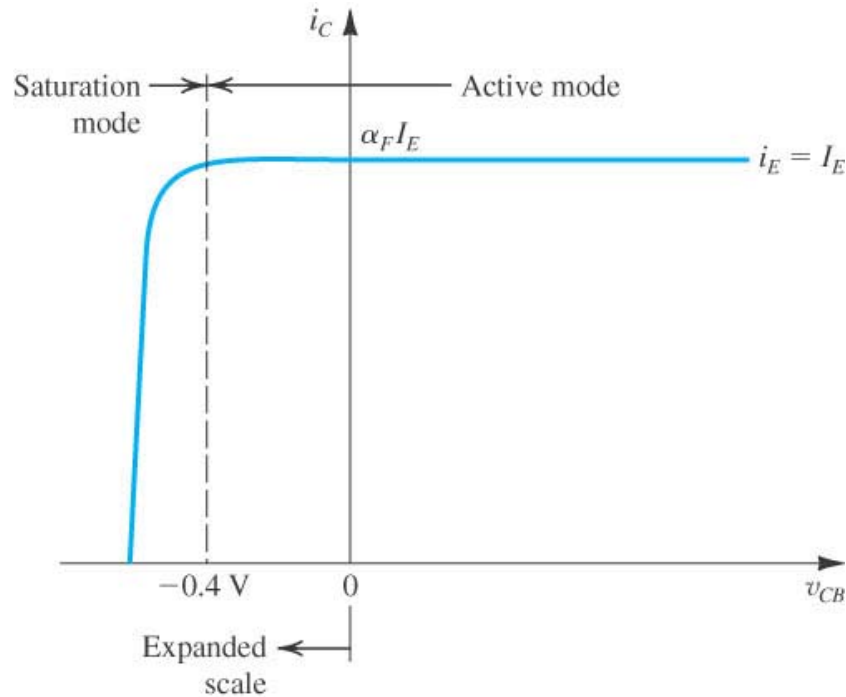
For $\beta = 100$, $\alpha = 100/101 = 0.99 \rightarrow I_E = I_C / \alpha = 2 / 0.99 = 2.02$ mA

$$\text{Now, } R_E = \frac{V_E - (-15)}{I_E} = \frac{-0.717 + 15}{2.02} = 7.07 \text{ k}\Omega$$

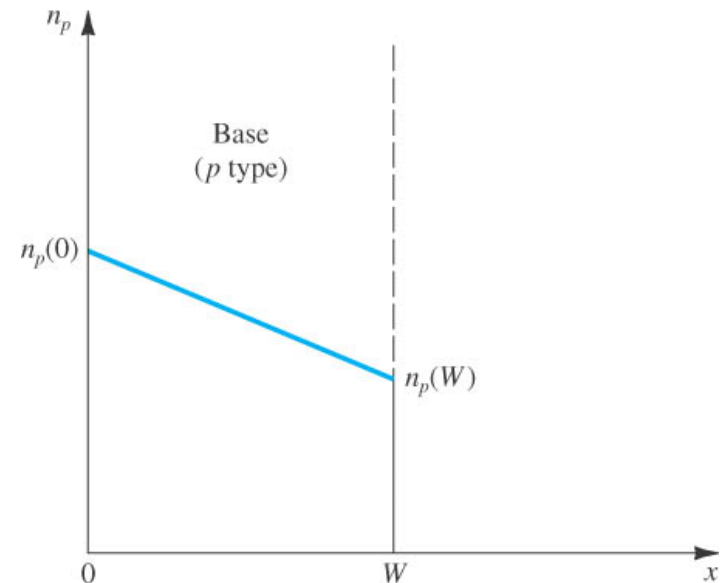
This order of accuracy is not necessary

Operation in the Saturation Mode

IV Characteristics



Minority Carrier Profile



- Forward active region can be maintained for negative v_{CB} down to about -0.4 V
- Beyond that point, the transistor enters the saturation mode and i_C decreases with decreasing v_{CB}

Operation in the Saturation Mode

If v_{BC} increases, i_C will decrease, as described by

$$i_C = I_S \left(e^{v_{BE}/V_T} - 1 \right) - \left(\frac{I_S}{\alpha_R} \right) \left(e^{v_{BC}/V_T} - 1 \right)$$

The base current i_B will decrease, as described by

$$i_B = \left(\frac{I_S}{\beta_F} \right) \left(e^{v_{BE}/V_T} - 1 \right) + \left(\frac{I_S}{\beta_R} \right) \left(e^{v_{BC}/V_T} - 1 \right)$$

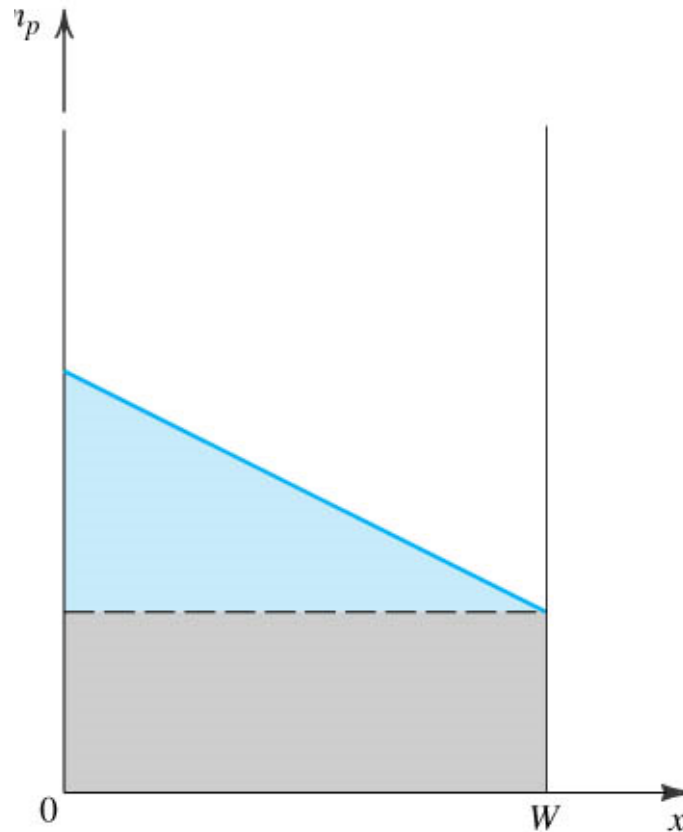
The current gain will decrease to a value lower than β_F described as:

$$\beta_{forced} = \left. \frac{i_C}{i_B} \right|_{saturation} \leq \beta_F$$

We will also have:

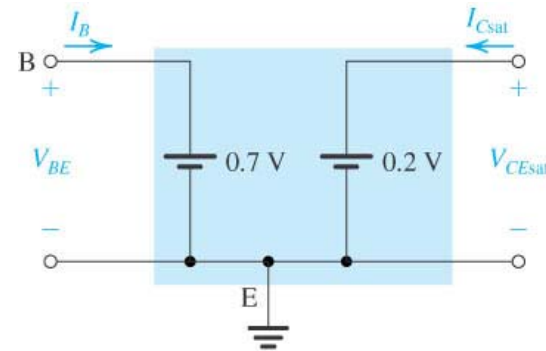
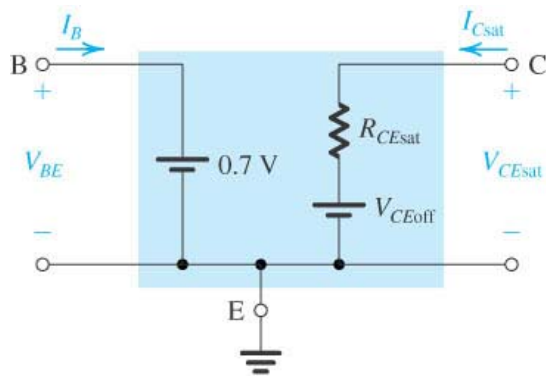
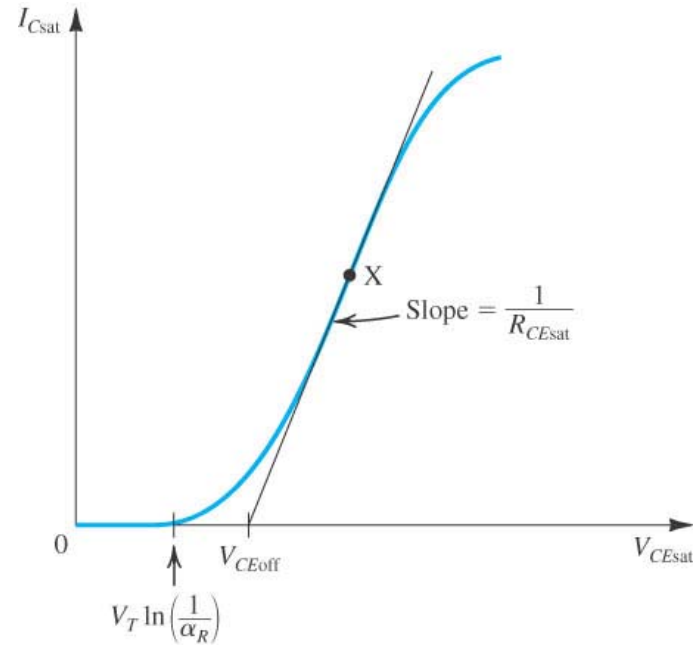
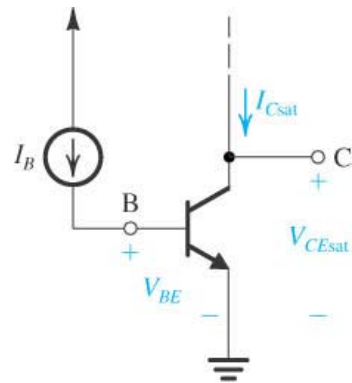
$$V_{CEsat} = V_{BE} - V_{BC}$$

Operation in the Saturation Mode

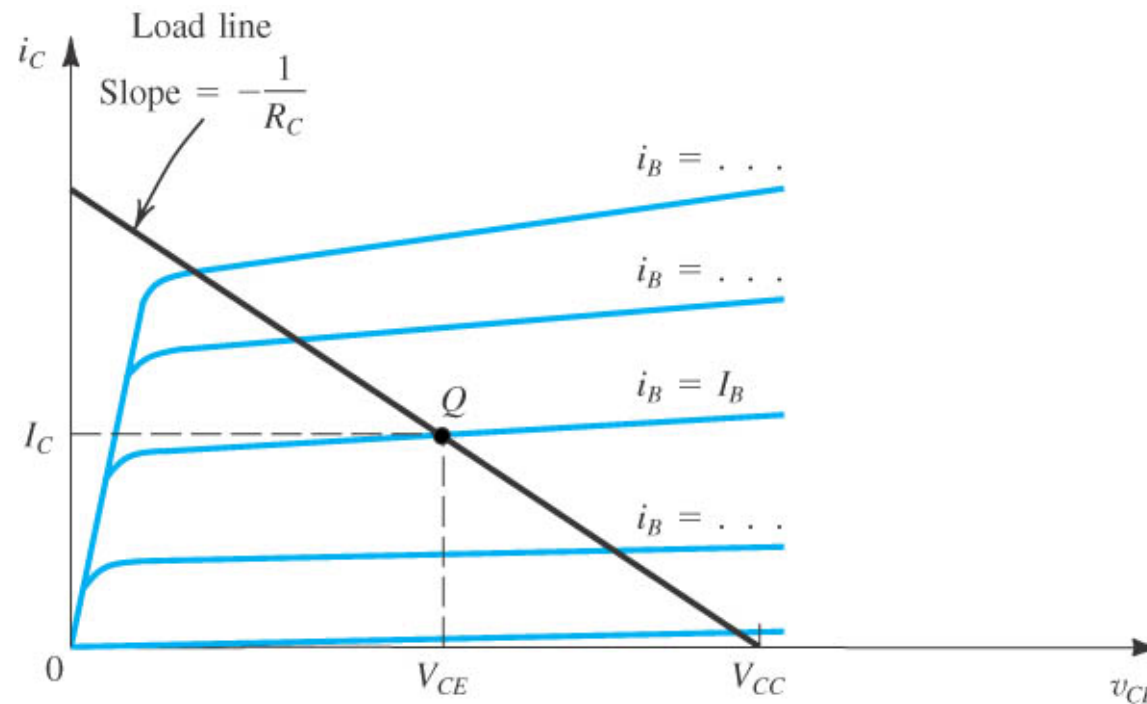


- Blue: Gradient that gives rise to diffusion current
- Gray: Minority carriers driving transistor deeper into saturation

NPN in Saturation Mode

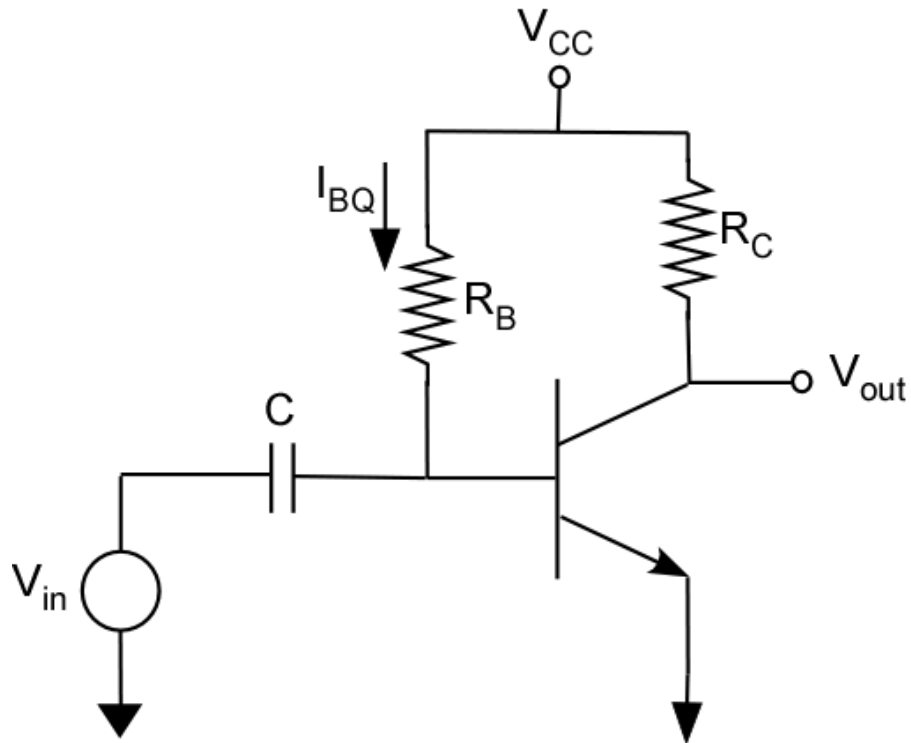


Biassing Bipolar Transistors



BJT Bias

1. Base Current Bias



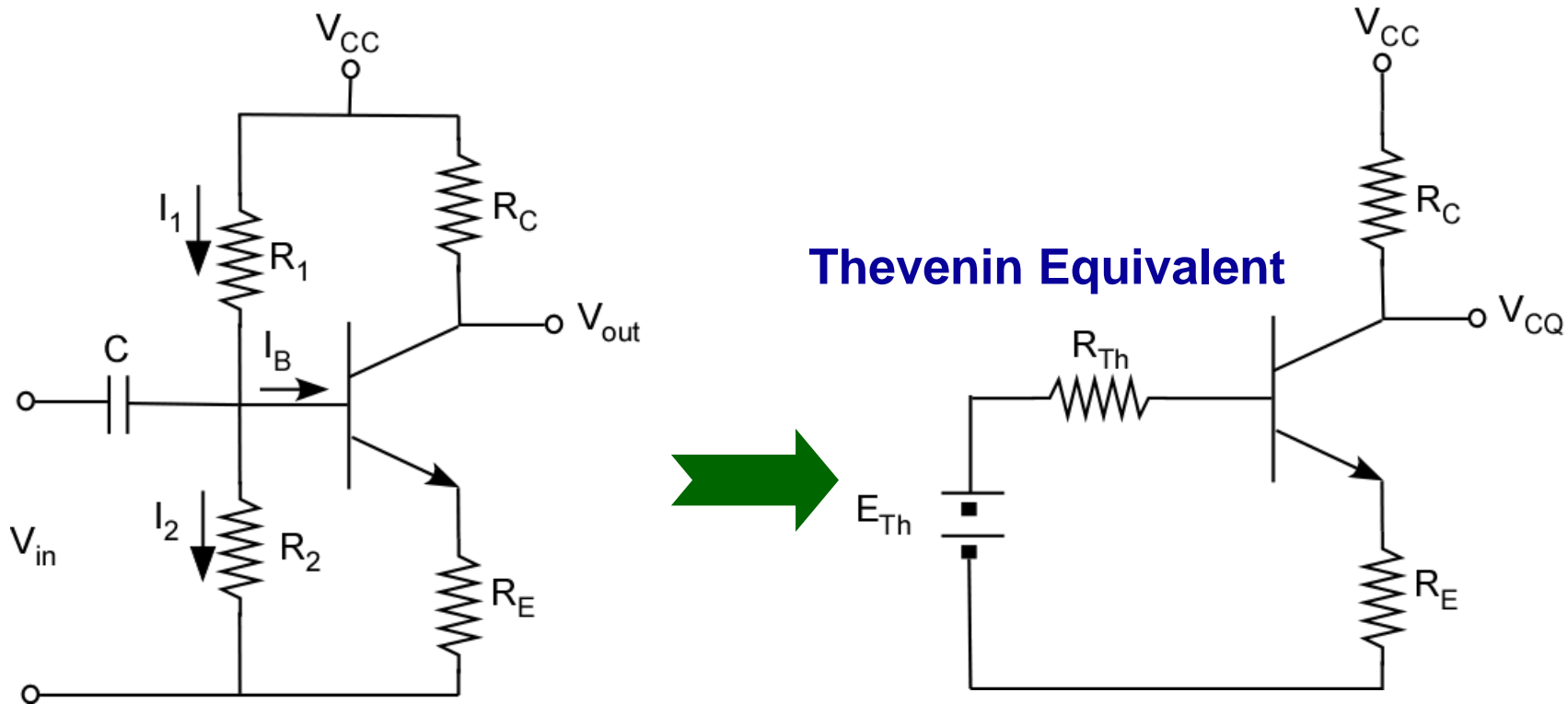
$$I_{BQ} = \frac{V_{CC} - V_{BE}}{R_B}$$

$$I_{BQ} = \frac{V_{CC} - 0.6}{R_B}$$

$$I_{BQ} \approx \frac{V_{CC}}{R_B}$$

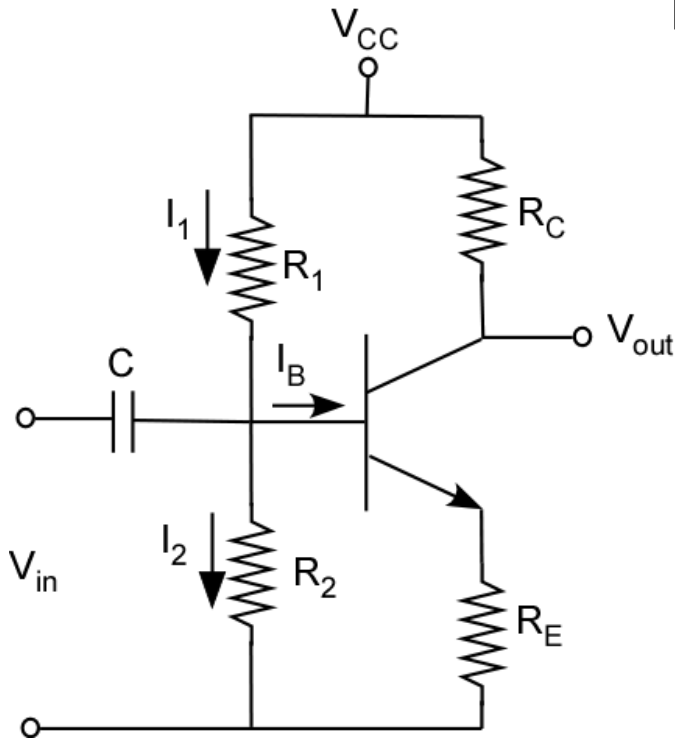
BJT Bias

2. Emitter Bias



Provides good stability with respect to changes in β with temperature

BJT Emitter Bias



$$E_{th} = R_{th} I_B + V_{BE} + R_E I_E$$

$$I_E = I_B + I_C = (\beta + 1) I_B$$

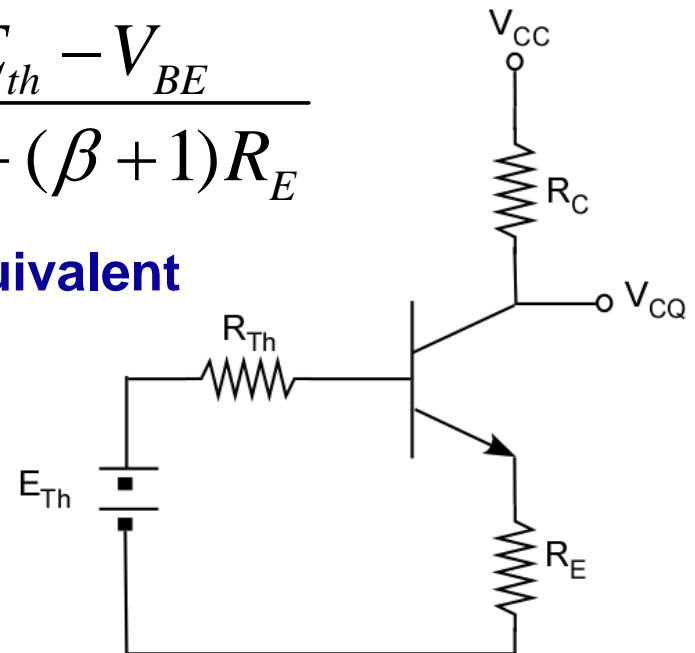
$$E_{th} - V_{BE} = R_{th} I_B + R_E (\beta + 1) I_B$$

$$I_B = I_{BQ} = \frac{E_{th} - V_{BE}}{R_{th} + (\beta + 1) R_E}$$

$$E_{th} = \frac{R_2}{R_1 + R_2} V_{CC}$$

$$R_{th} = R_1 \parallel R_2 = \frac{R_1 R_2}{R_1 + R_2}$$

Thevenin Equivalent



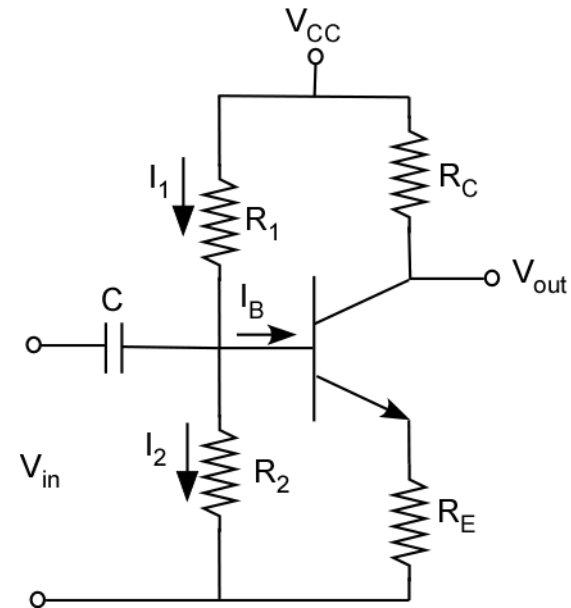
Bipolar Biasing Approach

- **Methods**

- First method is to find R_1 & R_2 from E_{th} and R_{th} and I_{BQ}
- Second method is to select R_2 to be 10 times to 20 times R_E to provide good stability & then select R_1 to give proper I_{BQ}

Remark: To keep collector voltage at the middle of the forward active region, use:

$$V_{CQ} = \frac{V_{Cmin} + V_{Cmax}}{2} = \frac{V_{CC}}{2} \left(1 + \frac{R_E}{R_E + R_C} \right)$$



Stability Considerations

Objective: Minimize effect of variations in β . Circuit must be stable with respect to changes in β .

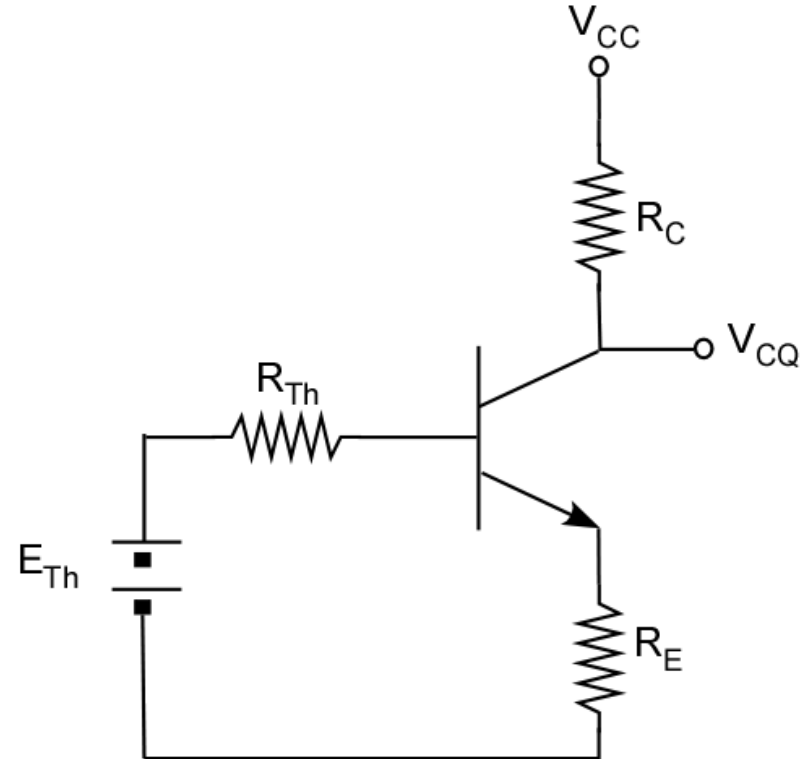
- Need to examine quiescent point in variations for interchanged BJT's

$$V_{CQ} = V_{CC} - I_{CQ}R_C = V_{CC} - \beta I_{BQ}R_C$$

$$R_{th}I_{BQ} + (\beta + 1)I_{BQ}R_E = E_{th} - V_{BE}$$

$$I_{BQ} = \frac{E_{th} - V_{BE}}{R_{th} + (\beta + 1)R_E}$$

$$V_{CQ} = V_{CC} - \frac{\beta(E_{th} - V_{BE})R_C}{R_{th} + (\beta + 1)R_E}$$



Stability Considerations

(A) If $R_{th} \gg (\beta+1)R_E$

$$V_{CQ} \approx V_{CC} - \frac{\beta R_C}{R_{th}} (E_{th} - V_{BE})$$

Changes in β lead to significant changes in V_{CQ}

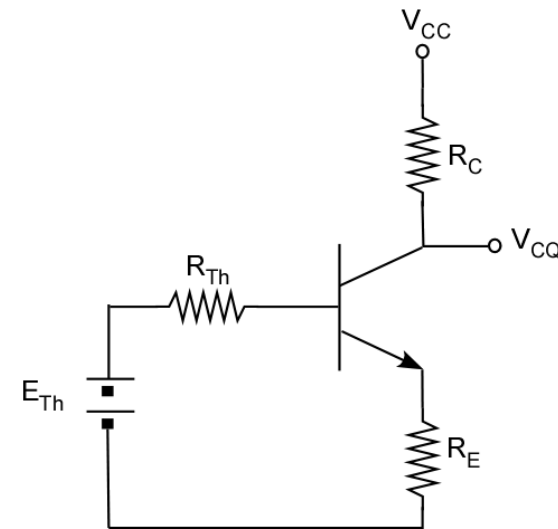
(B) If $(\beta+1)R_E \gg R_{th}$

$$V_{CQ} \approx V_{CC} - \frac{\beta R_C}{(\beta+1)R_E} (E_{th} - V_{BE})$$

$$V_{CQ} \approx V_{CC} - \frac{\alpha R_C}{R_E} (E_{th} - V_{BE})$$

$$\beta = 60 \Rightarrow \alpha = \frac{60}{61} = 0.983$$

$$\beta = 100 \Rightarrow \alpha = \frac{100}{101} = 0.99$$

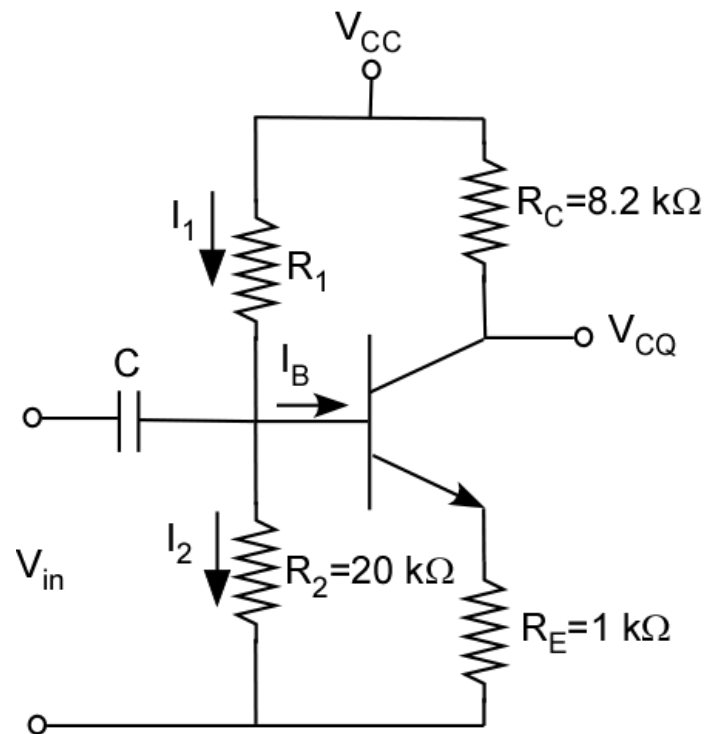


α varies only 1% to 2% for large β variations \rightarrow (B) is good choice.

Bias Example

The circuit shown below has $R_C = 8.2 \text{ k}\Omega$, $R_E = 1 \text{ k}\Omega$, $R_2 = 20 \text{ k}\Omega$, $V_{CC} = 12 \text{ V}$, $\beta = 100$, $V_{BE} = 0.7 \text{ V}$

- Select R_1 to place V_{CQ} at midpoint of the (forward) active region.
- Find maximum symmetrical peak-to-peak output voltage that can be obtained before saturation or cutoff occurs.



Bias Example - Solution

Minimum: $V_{CQ\min} = V_{CC} \frac{R_E}{R_E + R_C} = \frac{12}{1+8.2} = \frac{12}{9.2} = 1.3043 \text{ V}$

Maximum: $V_{CQ\max} = V_{CC}$

Midpoint: $V_{CQ} = \frac{V_{CQ\min} + V_{CQ\max}}{2} = \frac{1.3043 + 12}{2} = \frac{13.3043}{2} = 6.65 \text{ V}$

$$I_{CQ} = \frac{12 - 6.65}{R_C} = 0.652 \text{ mA}$$

$$I_{BQ} = \frac{0.652}{100} = 0.00652 \text{ mA} = 6.52 \mu\text{A}$$

Bias Example (con't)

$$V_{BQ} = R_E I_E + 0.7 = 0.652 + 0.7 = 1.35 \text{ V}$$

$$I_2 = \frac{1.35 \text{ V}}{20 \text{ k}\Omega} = 0.0676 \text{ mA} = 67.6 \mu\text{A}$$

$$I_1 = I_2 + I_B = 67.6 \mu\text{A} + 6.82 \mu\text{A} = 74.1 \mu\text{A}$$

$$R_1 = \frac{V_{CC} - 1.35}{I_1} = \frac{12 - 1.35}{74.1 \mu\text{A}} = 143.6 \text{ k}\Omega$$

$$V_{\max} = 12 - 6.65 = 5.35 \text{ V}$$

$$R_1 = 143.6 \text{ k}\Omega$$

$$V_{\max} = 5.35 \text{ V}$$