



An Introduction to X-Parameters*

ECE 451: Advanced Microwave Measurements

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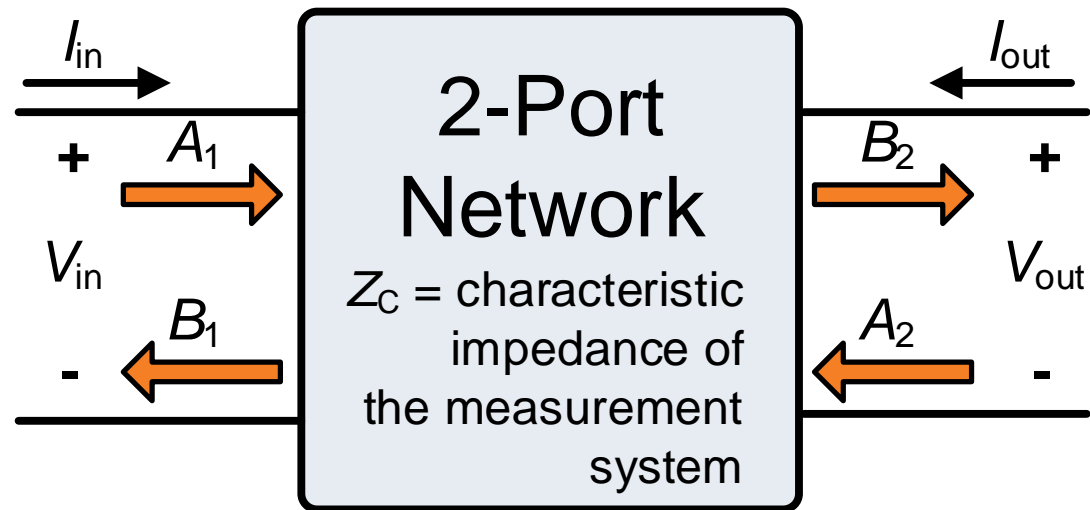
Scattering Parameters

$$A_1 = \frac{(V_{in} + Z_C I_{in})}{2\sqrt{Z_C}} \quad A_2 = \frac{(V_{out} + Z_C I_{out})}{2\sqrt{Z_C}}$$

$$B_1 = \frac{(V_{in} - Z_C I_{in})}{2\sqrt{Z_C}} \quad B_2 = \frac{(V_{out} - Z_C I_{out})}{2\sqrt{Z_C}}$$

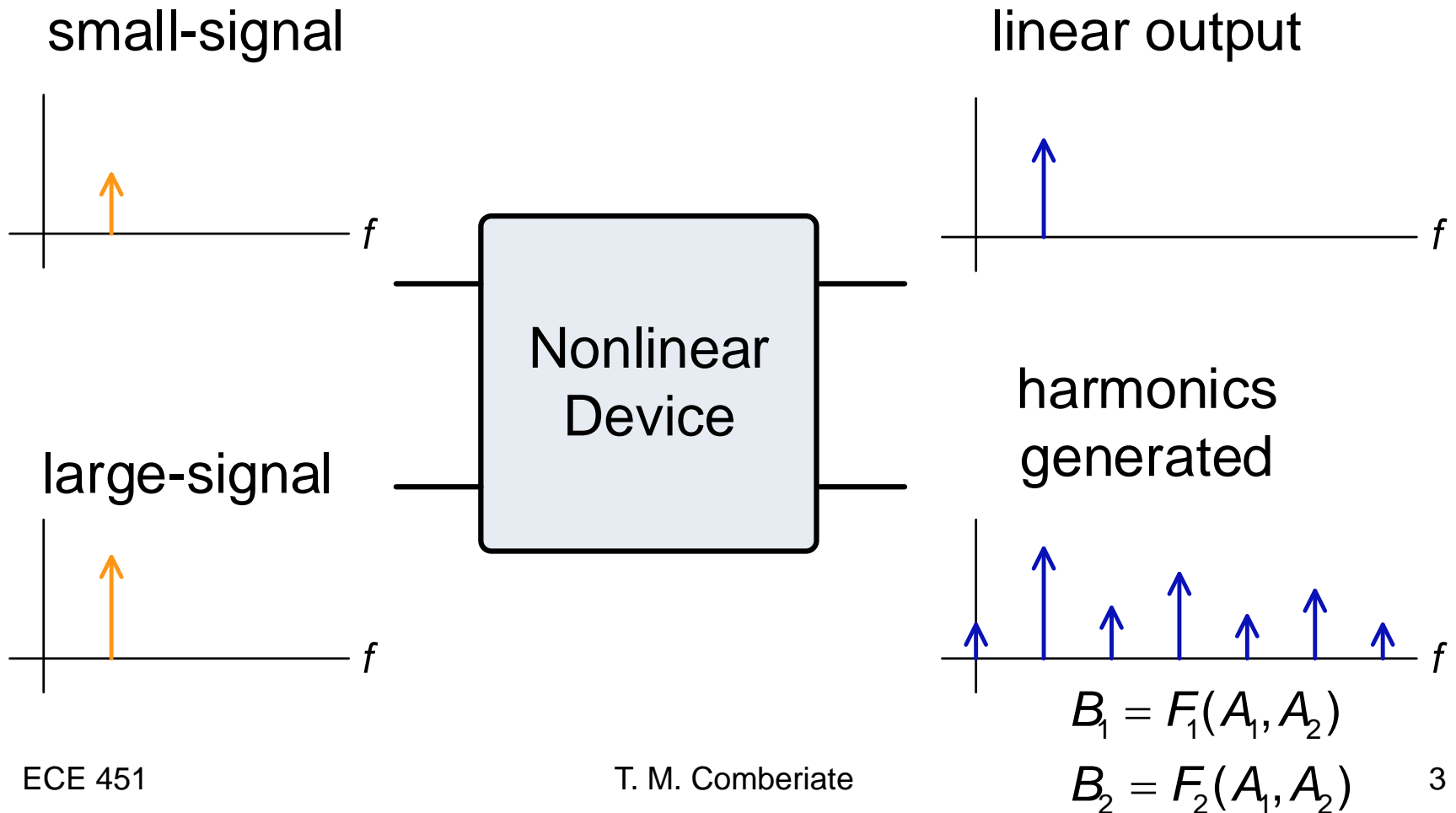
$$B_1 = S_{11}A_1 + S_{12}A_2$$

$$B_2 = S_{21}A_1 + S_{22}A_2$$

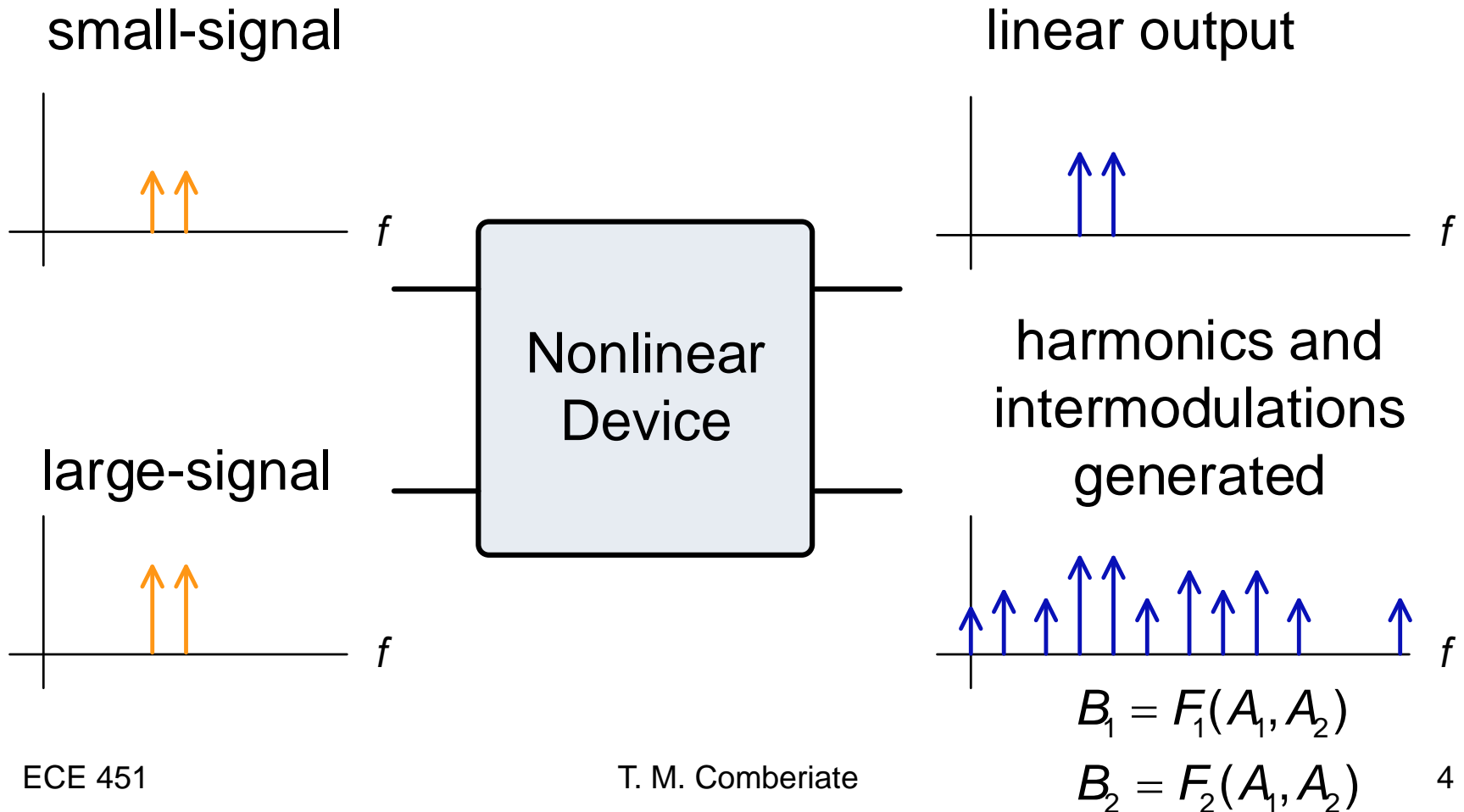


- Models all linear time-invariant behavior.
- Can model time-invariant nonlinear devices in the small-signal case.
- What about the large-signal case?

Nonlinear Functions with Single-Tone Stimuli

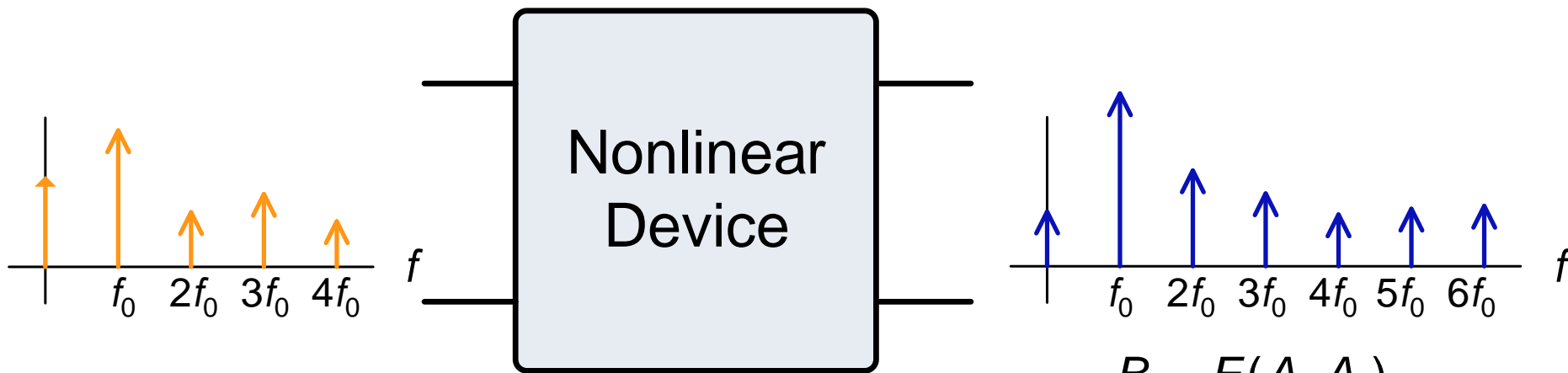


Nonlinear Functions with Multi-Tone Stimuli



Nonlinear Functions with Commensurate Tone Stimuli

- A set of pure tones are commensurate if all the tones in the set are located on a frequency grid $f_k = kf_0$ defined by f_0 , called the fundamental.
- Output tones will all land on the same frequency grid and have a same common period.

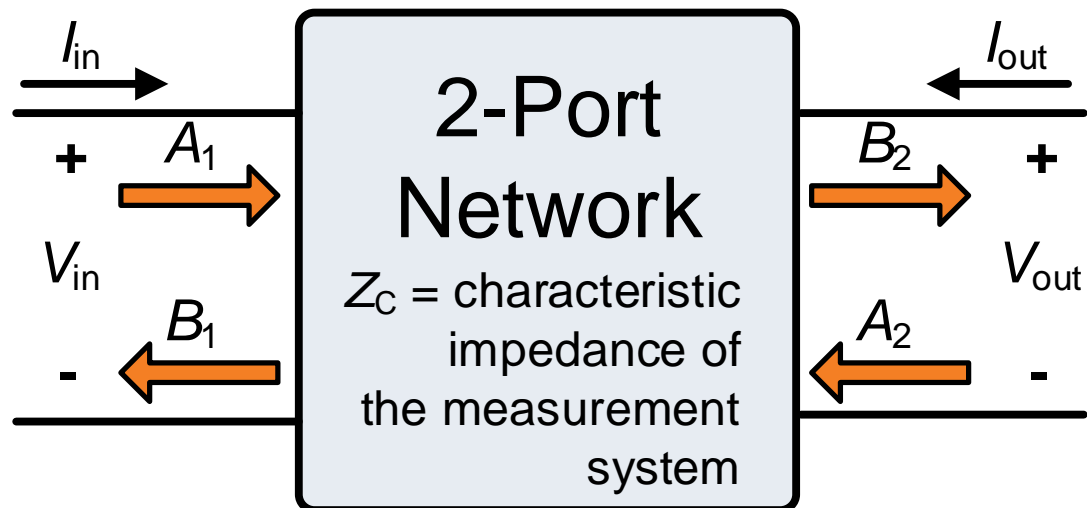


$$B_1 = F_1(A_1, A_2)$$

$$B_2 = F_2(A_1, A_2)$$

Nonlinear Scattering Waves

- Break incident and scattered waves into their commensurate tone components, called pseudowaves.



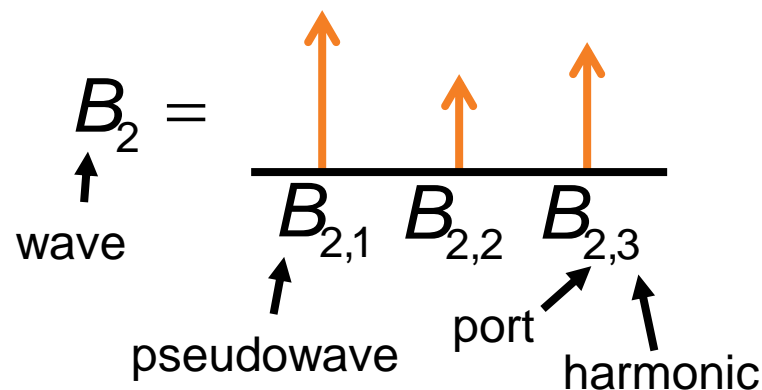
$$B_1 = F_1(A_1, A_2)$$

$$B_2 = F_2(A_1, A_2)$$



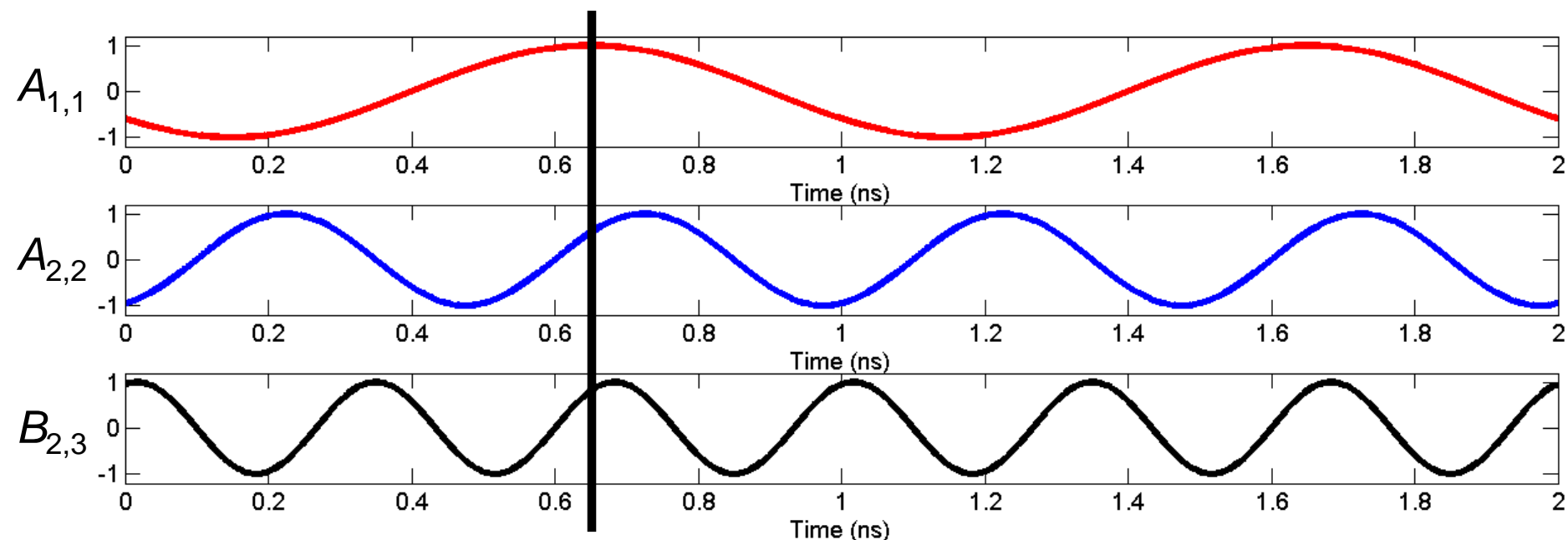
$$B_{1,k} = F_{1,k}(A_{1,1}, A_{1,2}, A_{1,3}, \dots, A_{2,1}, A_{2,2}, A_{2,3}, \dots)$$

$$B_{2,k} = F_{2,k}(A_{1,1}, A_{1,2}, A_{1,3}, \dots, A_{2,1}, A_{2,2}, A_{2,3}, \dots)$$

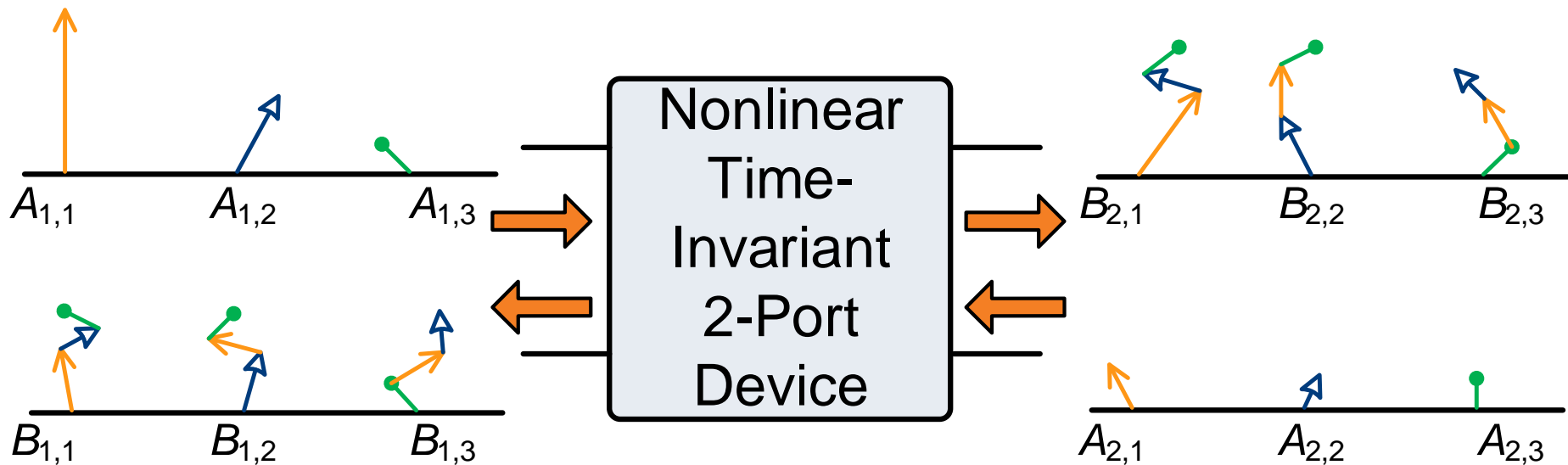


Cross-Frequency Phase for Commensurate Tones

- Defined as the phase of each pseudowave when the fundamental, $A_{1,1}$, has zero phase.
- $B_{2,3}$ can be related to $A_{2,2}$ in magnitude and phase.



Nonlinear Scattering Functions



$$B_{p,k} = F_{p,k}(A_{1,1}, A_{1,2}, A_{1,3}, \dots, A_{2,1}, A_{2,2}, A_{2,3}, \dots)$$

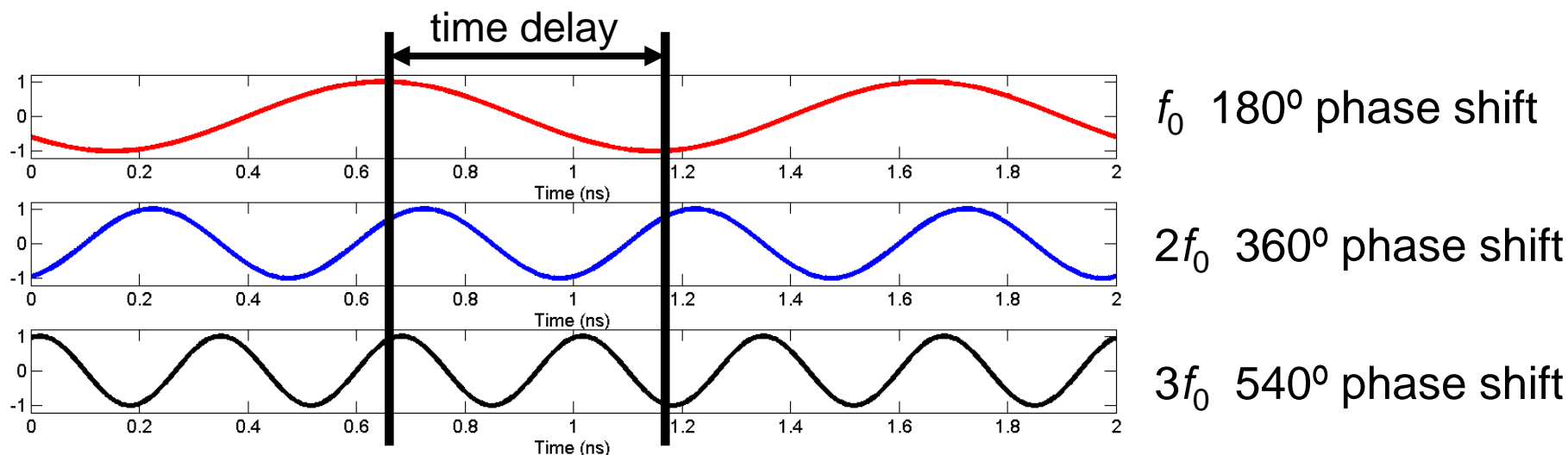
- Scattered pseudowave determined by a complicated time-invariant scattering function that depends on the magnitude and phase of each incident pseudowave.

Time-Invariance Property of Nonlinear Scattering Function

$$F_{p,k}(A_{1,1} e^{j\theta}, A_{1,2} (e^{j\theta})^2, A_{1,3} (e^{j\theta})^3, \dots)$$

$$= F_{p,k}(A_{1,1}, A_{1,2}, A_{1,3}, \dots) (e^{j\theta})^k$$

- Shifting all of the inputs by the same time means that different harmonic components are shifted by different phases.



Defining Phase Reference

- Can use time-invariance to separate magnitude and phase dependence of one incident pseudowave.

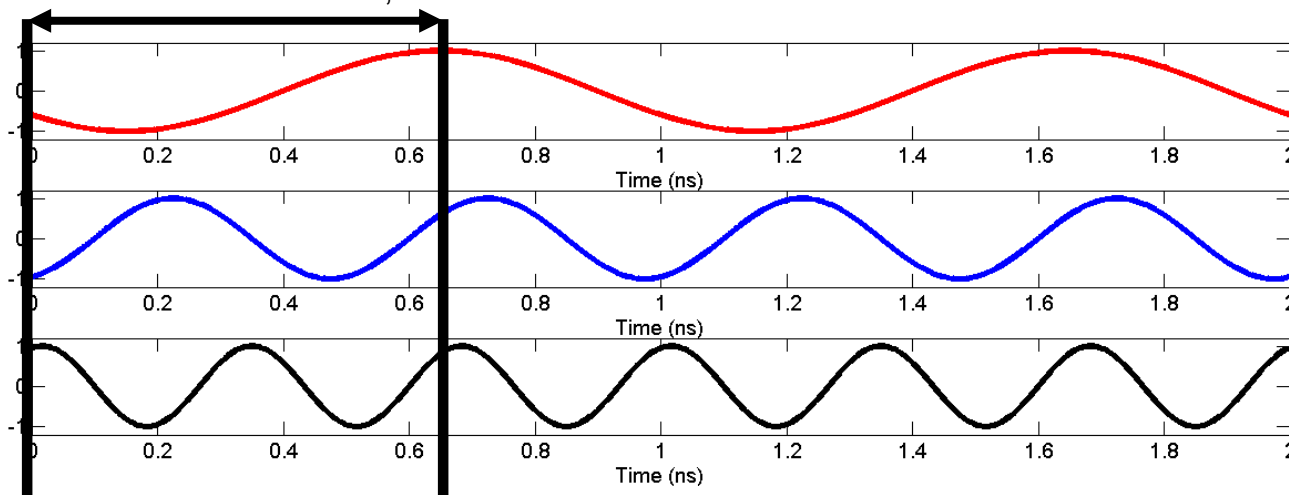
$$B_{p,k} = F_{p,k}(A_{1,1}, A_{1,2}, A_{1,3}, \dots)$$

using

$$= F_{p,k}(|A_{1,1}|, A_{1,2}P^{-2}, A_{1,3}P^{-3}, \dots)P^k$$

$$P = \frac{A_{1,1}}{|A_{1,1}|} = e^{j\arg(A_{1,1})}$$

Shifting reference to zero phase of $A_{1,1}$.



Commensurate Tones

X-Parameter Formalism

- Define $X_{p,k}^{(FB)}(|A_{1,1}|, A_{1,2}P^{-2}, A_{1,3}P^{-3}, \dots)$
 $= F_{p,k}(A_{1,1}, A_{1,2}, A_{1,3}, \dots)P^{-k}$



$$B_{p,k} = X_{p,k}^{(FB)}(|A_{1,1}|, A_{1,2}P^{-2}, A_{1,3}P^{-3}, \dots)P^k$$

- Still difficult to characterize this nonlinear term.
- If only one incident pseudowave, $A_{1,1}$, is large then the other smaller inputs can be linearized about the large-signal response of $F_{p,k}$ to only $A_{1,1}$.

Linearization of $F_{p,k}$ about $A_{1,1}$

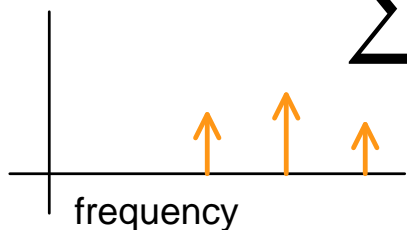
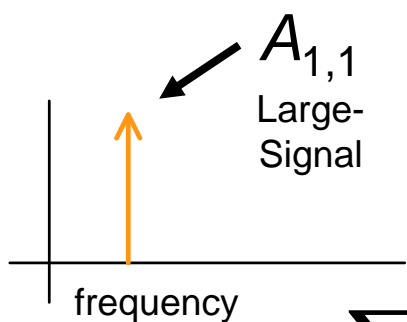
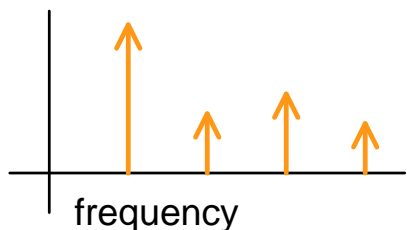
$$B_{p,k} = F_{p,k} \left(|A_{1,1}|, A_{1,2}P^{-2}, \dots, A_{1,K}P^{-K}, \dots \right) P^k$$

$$\approx F_{p,k} \left(|A_{1,1}|, 0, \dots, 0, \dots \right) P^k$$

$$+ \sum_{\substack{q=1, l=1 \\ (q,l) \neq 1}}^{q=N, l=K} \left[\underbrace{\frac{\partial F_{p,k}}{\partial (A_{q,l}P^{-l})} \Big|_{|A_{1,1}|}}_{X^{(S)}_{p,k;q,l}} A_{q,l} P^{k-l} + \frac{\partial F_{p,k}}{\partial \left((A_{q,l}P^{-l})^* \right)} \Big|_{|A_{1,1}|}}_{X^{(T)}_{p,k;q,l}} A_{q,l}^* P^{k+l} \right]$$

1-Tone X-Parameter Formalism

Incident Waves



Approximates

$$B_{p,k} = X_{p,k}^{(FB)}(|A_{1,1}|, A_{1,2}P^{-2}, A_{1,3}P^{-3}, \dots)$$

Nonlinear Mapping

\approx

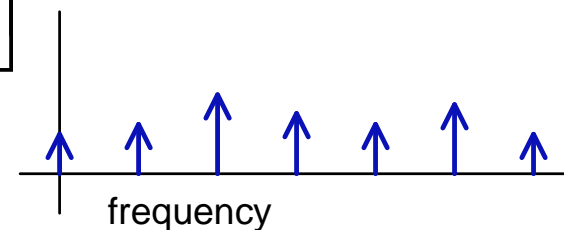
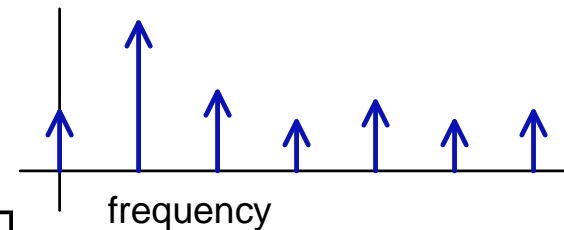
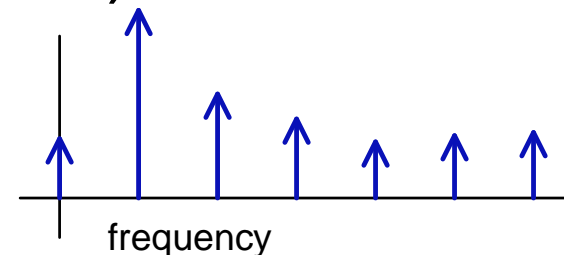
$$X_{p,k}^{(FB)}(|A_{1,1}|, 0, 0, \dots)$$

Simple Nonlinear Mapping

$$\sum \left[X_{p,k;q,l}^{(S)} \cdot A_{q,l} + X_{p,k;q,l}^{(T)} \cdot A_{q,l}^* \right]$$

Nonanalytic Harmonic
Superposition

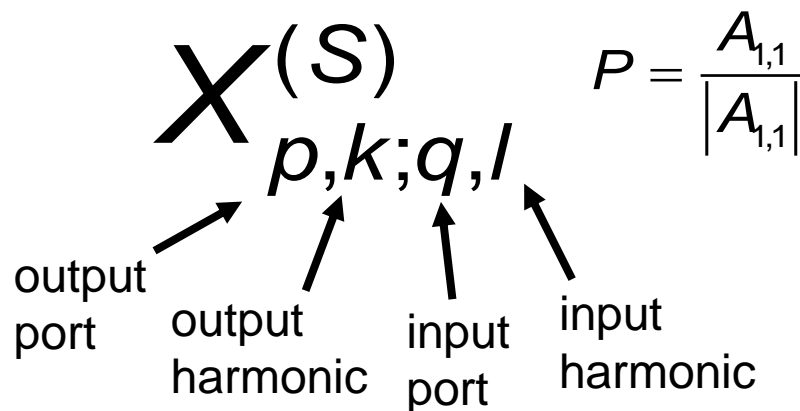
Scattered Waves



1-Tone X-Parameter Formalism

$$B_{p,k} \approx \underbrace{X_{p,k}^{(FB)} \cdot P^k}_{\text{Simple nonlinear map}} + \underbrace{\sum_{\substack{q=1, l=1 \\ (q,l) \neq (1,1)}}^{q=N, l=K} X_{p,k;q,l}^{(S)} \cdot A_{q,l} \cdot P^{k-l}}_{\text{Linear harmonic map function of incident wave}} + \underbrace{\sum_{\substack{q=1, l=1 \\ (q,l) \neq (1,1)}}^{q=N, l=K} X_{p,k;q,l}^{(T)} \cdot A_{q,l}^* \cdot P^{k+l}}_{\text{Linear harmonic map function of conjugate of incident wave}}$$

- X-parameters of type FB, S, and T fully characterize the nonlinear function.
- Depend on
 - frequency
 - large signal magnitude, $|A_{1,1}|$
 - DC bias



X-Parameters Collapse to S-Parameters in Small-Signal Limit

$$B_{p,k} \approx X_{p,k}^{(FB)} \cdot P^k + \sum_{\substack{q=1, l=1 \\ (q,l) \neq (1,1)}}^{q=N, l=K} X_{p,k;q,l}^{(S)} \cdot A_{q,l} \cdot P^{k-l} + \sum_{\substack{q=1, l=1 \\ (q,l) \neq (1,1)}}^{q=N, l=K} X_{p,k;q,l}^{(T)} \cdot A_{q,l}^* \cdot P^{k+l}$$

As $A_{1,1}$ shrinks, the conjugate terms and harmonic terms vanish:

$$B_{p,1} \approx X_{p,1}^{(FB)} \cdot P + \sum_{q=2}^{q=N} X_{p,1;q,1}^{(S)} \cdot A_{q,1}$$

Remove unnecessary harmonic index and assume 2-port:

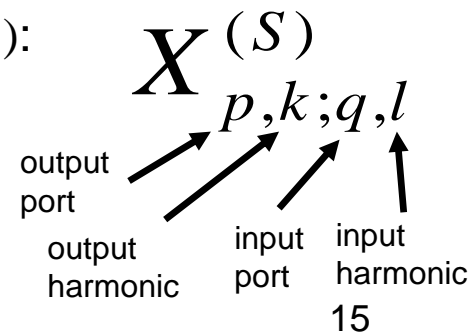
$$B_1 \approx X_1^{(FB)} \cdot P + X_{1,2}^{(S)} \cdot A_2$$

$$B_2 \approx X_2^{(FB)} \cdot P + X_{2,2}^{(S)} \cdot A_2$$

$$X_p^{(FB)} \cdot P = S_{p1} |A_1| P = S_{p1} A_1 \text{ for small } A_1 \text{ and } P \equiv \arg(A_1):$$

$$B_1 = S_{11} A_1 + S_{12} A_2$$

$$B_2 = S_{21} A_1 + S_{22} A_2$$





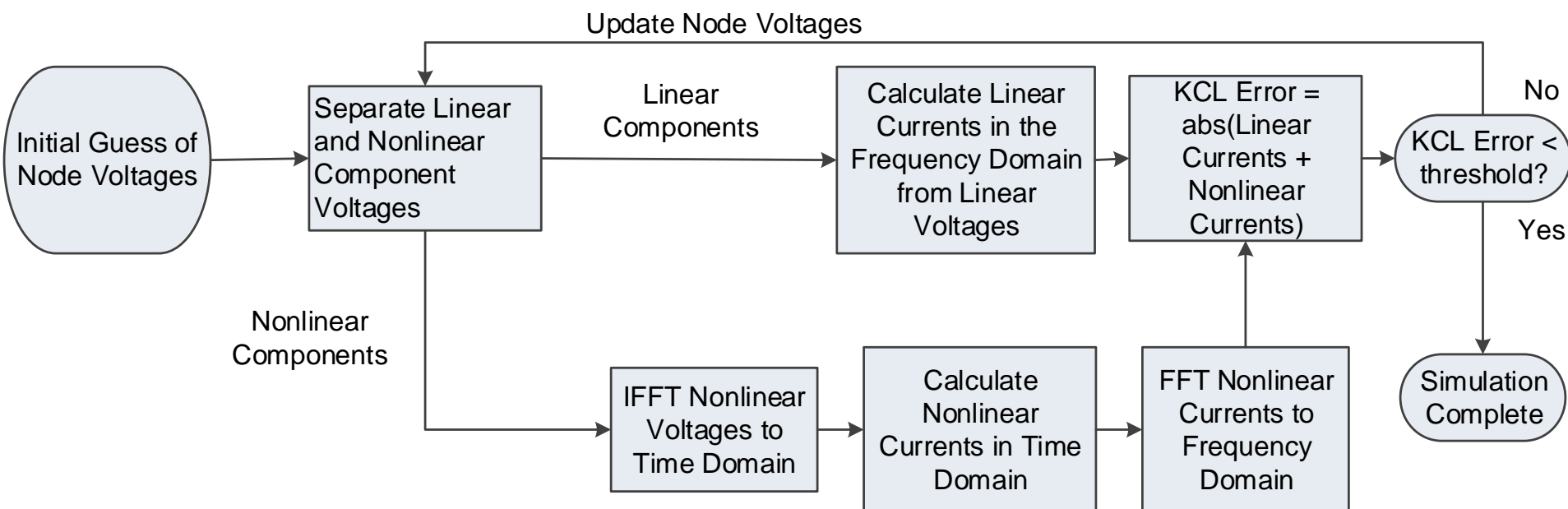
Generating X-Parameters

- Traditional Generation
 - Simulated using harmonic balance.
 - Measured with a nonlinear vector network analyzer (NVNA).

Harmonic Balance

Assume nodal voltages can be represented with Fourier series and solve for the Fourier coefficients.

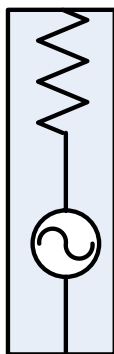
$$v(t) = \text{Re} \left[\sum_{k_1=0}^{K_1} \sum_{k_2=0}^{K_2} \cdots \sum_{k_n=0}^{K_n} V_{k_1, k_2, \dots, k_n} e^{j2\pi(k_1 f_1 + \dots + k_n f_n)t} \right]$$



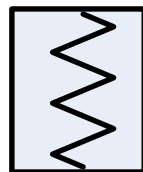
Generating X-Parameters with Harmonic Balance

- Need to set proper values for:
 - Frequency range
 - Fundamental power
 - DC bias
- X-parameter measurements are unidirectional because of large-signal fundamental $|A_{1,1}|$ on one port.
- Different types of X-parameter ports:

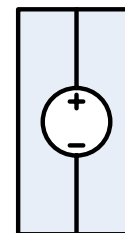
Source



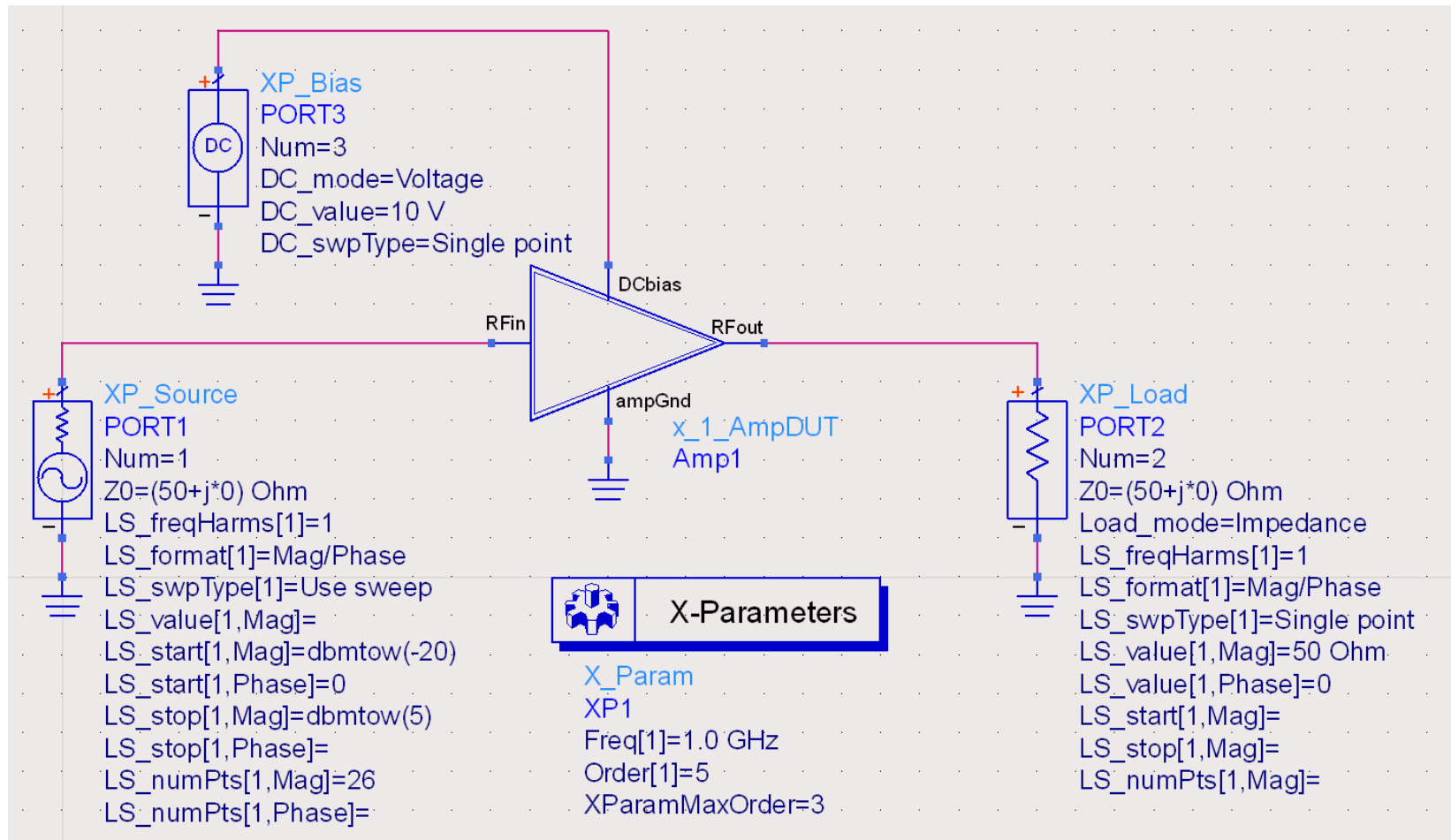
Load



Bias



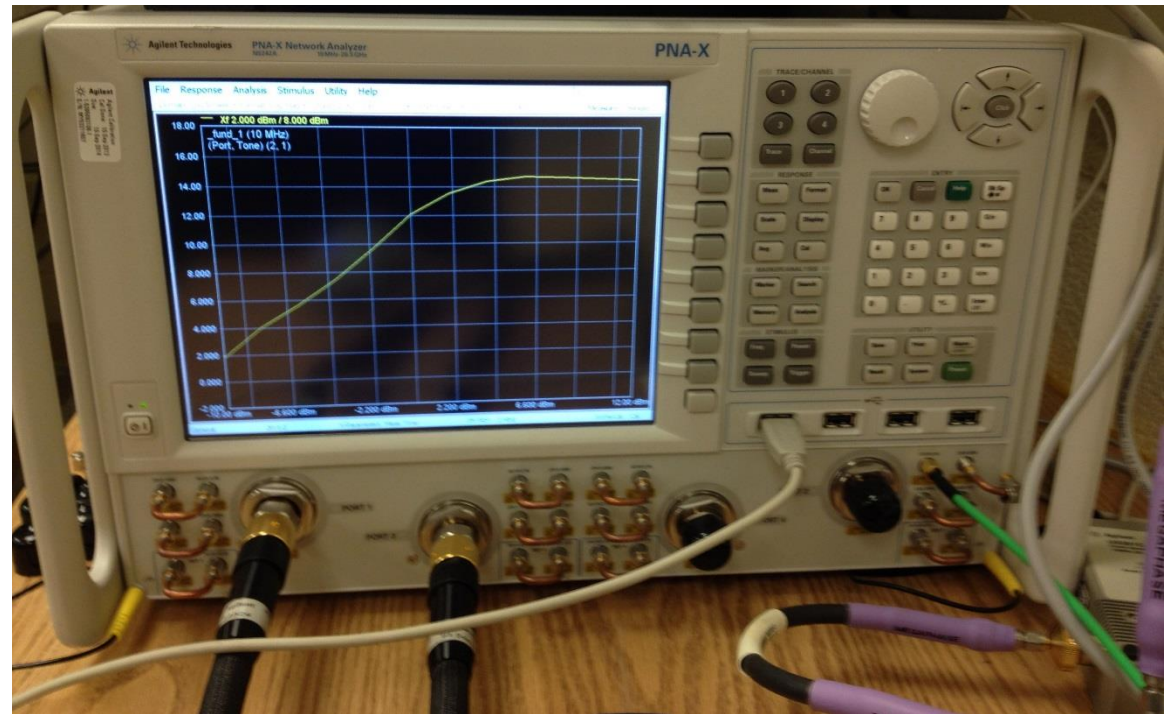
X-Parameter Generation Example



Nonlinear Vector Network Analyzer (NVNA)

PNA-X

- Four ports.
- Two filtered microwave sources.
- Microwave combiner.



Amplitude Calibration

- Necessary for any nonlinear measurement because linear property of homogeneity does not apply.
- Measures power and is controlled via GPIB.

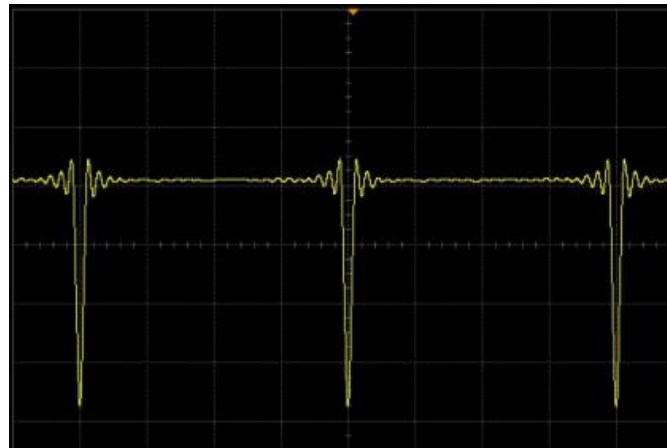


Phase Calibration

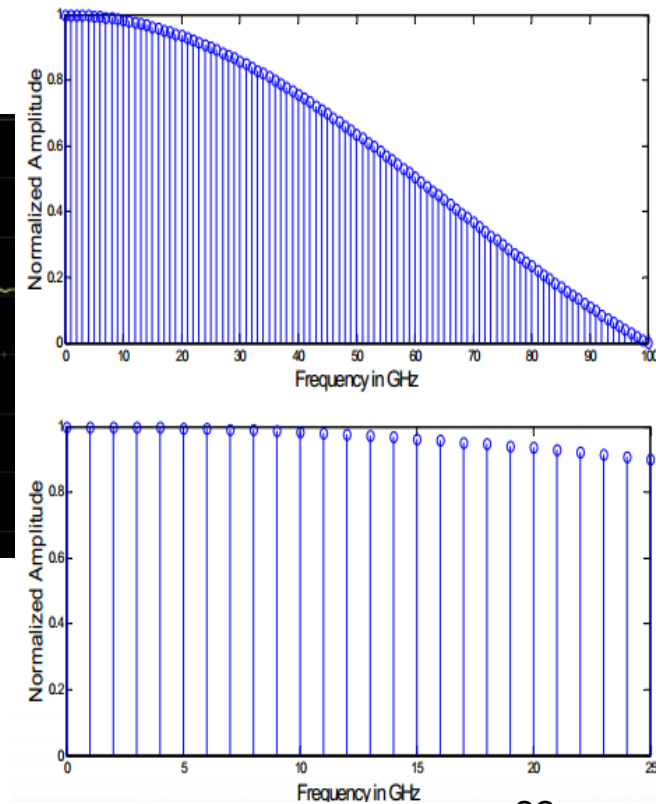
- Enables cross-frequency phase measurement.
- Takes frequency input from external microwave source.



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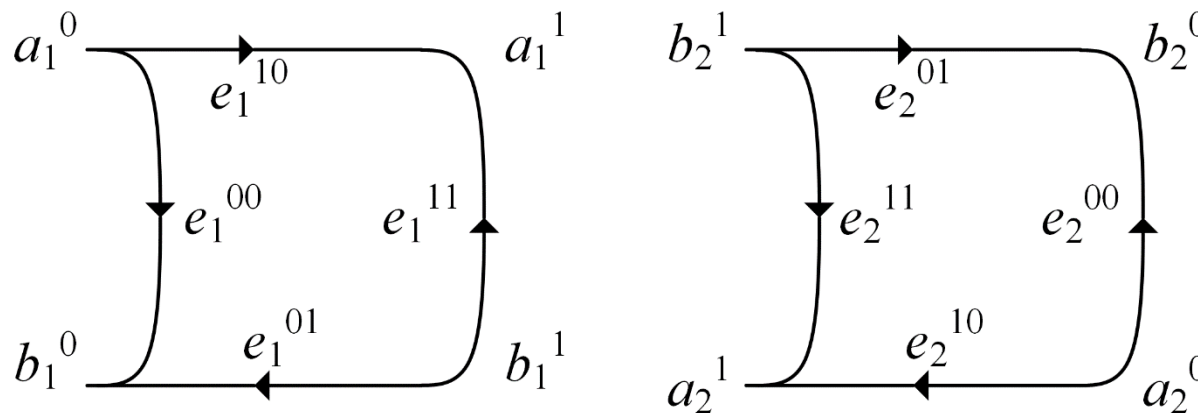
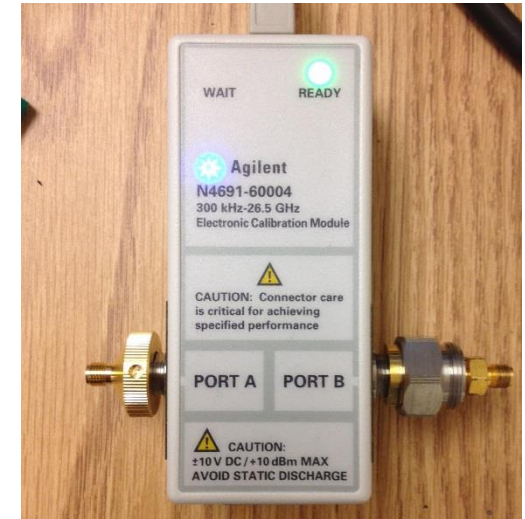


T. M. Comberiate



Vector Calibration

- Can use ECal.
- Based on eight-term error model.
- Works for forward, reverse, and combined stimuli.



Large-Signal X-Parameter Extraction

- Apply large-signal stimulus $A_{1,1}$ without any small-signal stimulus.
- Measure the response at all ports and harmonics of interest.
- $X_{p,k}^{(\text{FB})}$ term is the measured response to the large-signal stimulus at port p and harmonic k

Offset-Phase Small-Signal X-Parameter Extraction

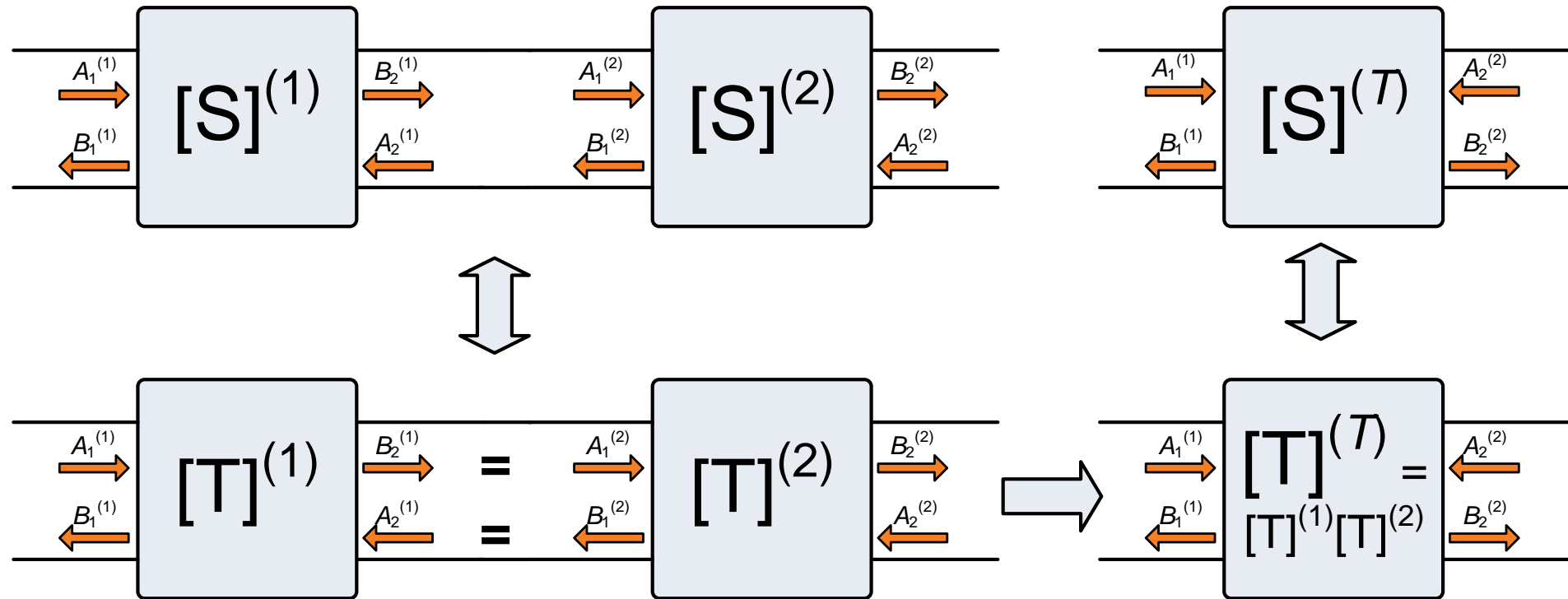
- Apply large-signal stimulus $A_{1,1}$ and one small-signal stimulus $A_{q,l}$ at zero phase.
- Measure the response at all ports and harmonics of interest.
- Apply large-signal stimulus $A_{1,1}$ and one small-signal stimulus $A_{q,l}$ at 90° phase.
- Measure the response at all ports and harmonics of interest.
- Use both measurements to extract

$$X_{p,k;q,l}^{(S)} \text{ and } X_{p,k;q,l}^{(T)}$$

Using X-Parameters

- Traditional Uses
 - Modeling mixers and amplifiers in steady-state simulations for RF systems.
 - Can be used to determine nonlinear figures of merit.
 - 1-dB Compression Point
 - AM/AM and AM/PM
 - Third Order Intercept

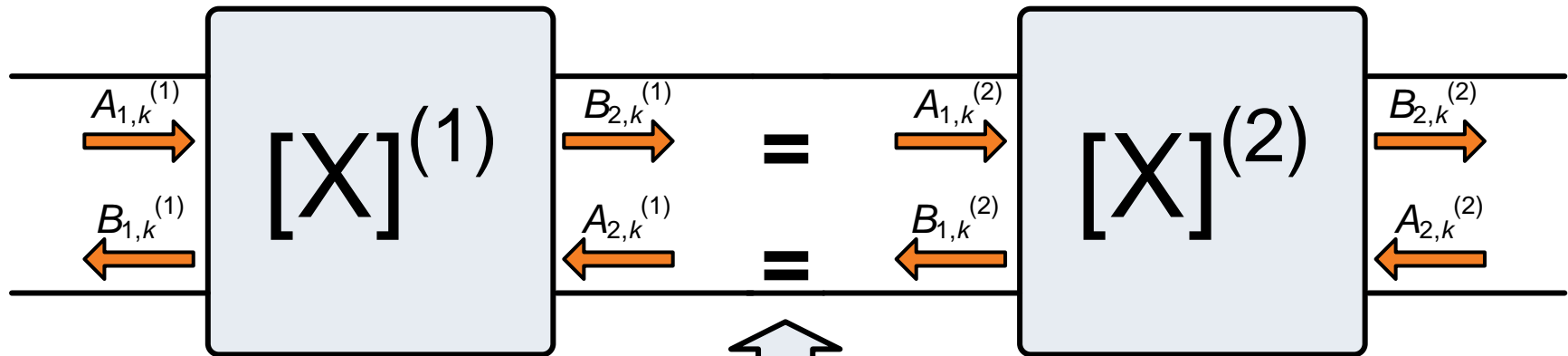
Cascading S-Parameter Blocks



$[T]$ = transfer scattering parameters.

Can disregard circuit behavior at internal node.

Cascading X-Parameter Blocks

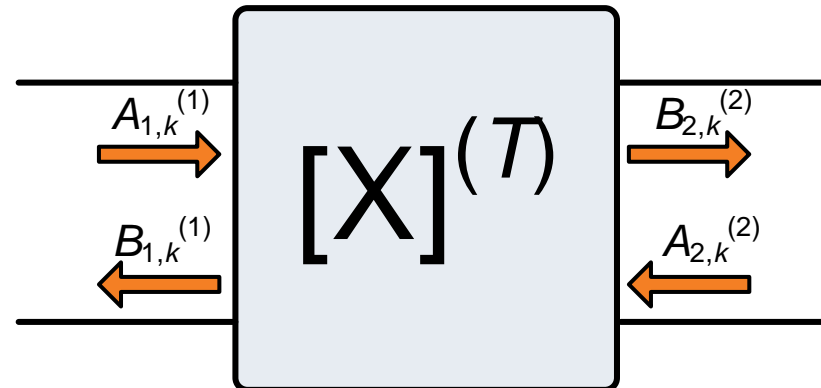


These equations at the internal node must always be satisfied:

$$B_{1,k}^{(1)} = A_{1,k}^{(2)},$$

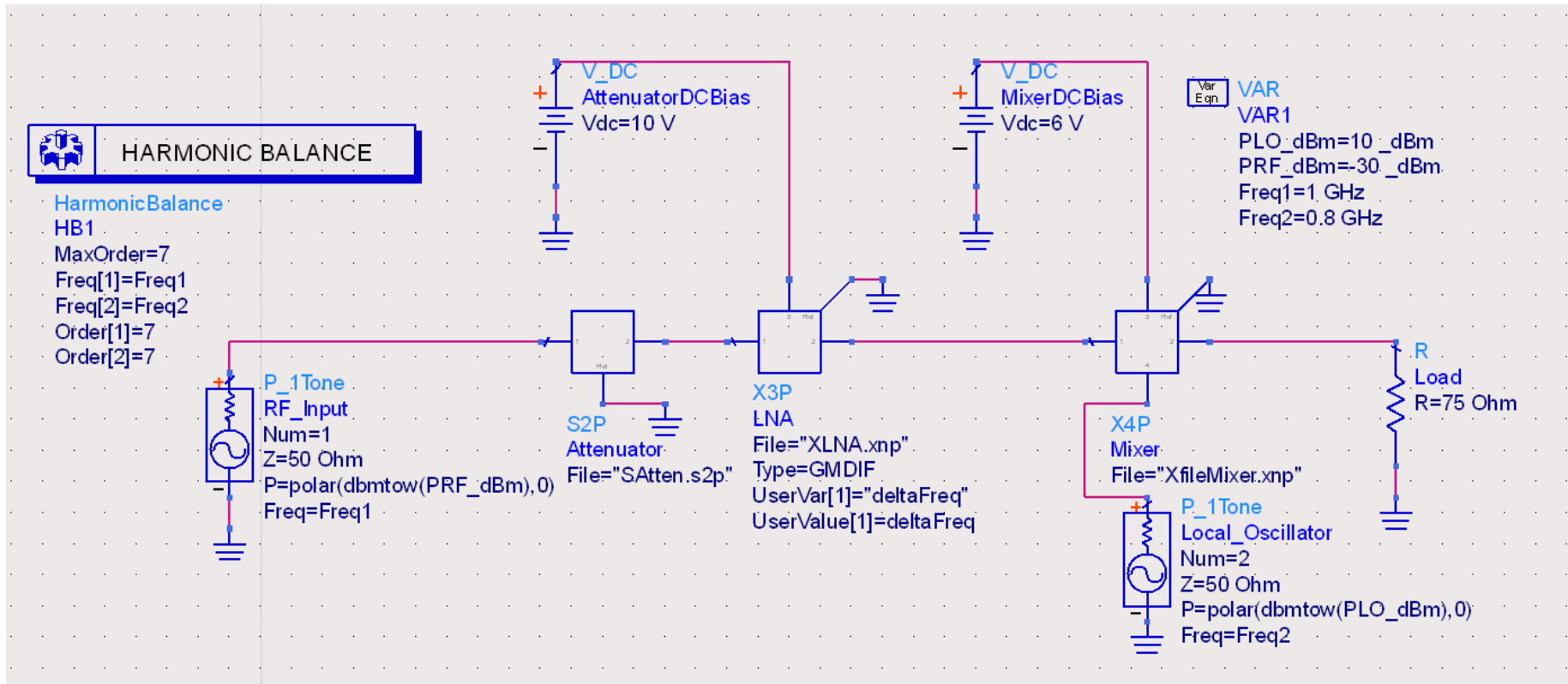
$$A_{1,k}^{(2)} = B_{2,k}^{(1)}$$

for all values of k .



Using X-Parameters in Simulation

Can construct entire receiver chains made of S- and X-parameter blocks.



X-Parameter Extensions

- Multiple Large Signals
- DC Components of Scattered Waves
 - DC current port bias: $X^{(Z)}_{p,k}$
 - DC voltage port bias: $X^{(Y)}_{p,k}$
- Memory Effects