ECE 451 Advanced Microwave Measurements

Requirements of Physical Channels

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Issues

- Frequency and time limitations
- Minimum phase characteristics
- Reality
- Stability
- Causality
- Passivity



Complex Plane

- An arbitrary network's transfer function can be described in terms of its s-domain representation
- -s is a complex number $s = \sigma + j\omega$
- The impedance (or admittance) or transfer function of networks can be described in the s domain as

$$T(s) = \frac{a_m s^m + a_{m-1} s^{m-1} + \dots + a_1 s + a_0}{s^n + b_{n-1} s^{n-1} + \dots + b_1 s + b_0}$$



Transfer Functions

$$T(s) = \frac{a_m s^m + a_{m-1} s^{m-1} + \dots + a_1 s + a_0}{s^n + b_{n-1} s^{n-1} + \dots + b_1 s + b_0}$$

The coefficients *a* and *b* are real and the order *m* of the numerator is smaller than or equal to the order *n* of the denominator

A stable system is one that does not generate signal on its own.

For a stable network, the roots of the denominator should have negative real parts



Transfer Functions

The transfer function can also be written in the form

$$T(s) = a_m \frac{(s - Z_1)(s - Z_2)...(s - Z_m)}{(s - P_1)(s - P_2)...(s - P_m)}$$

 $Z_1, Z_2, ...Z_m$ are the zeros of the transfer function

 $P_1, P_2, \dots P_m$ are the **poles** of the transfer function

For a stable network, the poles should lie on the left half of the complex plane



 $a_{re}(t)$: real part of even time-domain function

 $a_{ie}(t)$: imaginary part of even time-domain function

 $a_{ro}(t)$: real part of odd time-domain function

 $a_{io}(t)$: imaginary part of odd time-domain function

$$a(t) = a_{re}(t) + ja_{ie}(t) + a_{ro}(t) + ja_{io}(t)$$

In the frequency domain accounting for all the components, we can write:

 $A_{RE}(\omega)$: real part of even function in the frequency domain $A_{IE}(\omega)$: imaginary part of even function in the frequency domain $A_{RO}(\omega)$: real part of odd function in the frequency domain $A_{IO}(\omega)$: imaginary part of odd function in the frequency domain

$$A(\omega) = A_{RE}(\omega) + jA_{IE}(\omega) + A_{RO}(\omega) + jA_{IO}(\omega)$$



We also have the Fourier-transform-pair relationships:

Time Domain:
$$a(t) = a_{re}(t) + ja_{ie}(t) + a_{ro}(t) + ja_{io}(t)$$

$$\uparrow \qquad \uparrow \qquad \uparrow \qquad \qquad \searrow \qquad \qquad \searrow$$

Freq Domain:
$$A(\omega) = A_{RE}(\omega) + jA_{IE}(\omega) + A_{RO}(\omega) + jA_{IO}(\omega)$$

$$B(\omega) = S(\omega) \left[A_{RE}(\omega) + jA_{IE}(\omega) + A_{RO}(\omega) + jA_{IO}(\omega) \right]$$

In the time domain, this corresponds to:

$$b(t) = s(t) * \left[\left(a_{re}(t) + a_{ro}(t) \right) + j \left(a_{ie}(t) + a_{io}(t) \right) \right]$$



We now impose the restriction that in the time domain, the function must be real. As a result,

$$a_{ie}(t) = a_{io}(t) = 0$$
 which implies that: $A_{IE}(\omega) = A_{RO}(\omega) = 0$

The Fourier-transform pair relationship then becomes:

Time Domain:
$$a(t) = a_{re}(t) + a_{ro}(t)$$

$$\uparrow \qquad \uparrow \qquad \uparrow$$

$$\downarrow \qquad \downarrow \qquad \downarrow$$

Freq Domain:
$$A(\omega) = A_{RE}(\omega) + jA_{IO}(\omega)$$

The frequency-domain relations reduce to:

$$B(\omega) = S(\omega) \left[A_{RE}(\omega) + jA_{IO}(\omega) \right]$$



In summary, the general relationship is:

Time Domain:
$$b(t) = b_{re}(t) + jb_{ie}(t) + b_{ro}(t) + jb_{io}(t)$$

$$\uparrow \qquad \uparrow \qquad \uparrow \qquad \qquad \searrow \qquad \qquad \searrow$$

Freq Domain:
$$B(\omega) = B_{RE}(\omega) + jB_{IE}(\omega) + B_{RO}(\omega) + jB_{IO}(\omega)$$

But for a real system:

Freq Domain:
$$B(\omega) = B_{RE}(\omega) + jB_{IE}(\omega) + B_{RO}(\omega) + jB_{IO}(\omega)$$



So, in summary

Time Domain:
$$b(t) = b_e(t) + b_o(t)$$
 $\uparrow \qquad \uparrow \qquad \uparrow$
 $\downarrow \qquad \downarrow \qquad \downarrow$

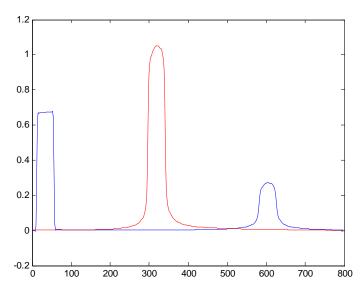
Freq Domain: $B(\omega) = B_R(\omega) + jB_I(\omega)$

The real part of the frequency-domain transfer function is associated with the even part of the time-domain response

The imaginary part of the frequency-domain transfer function is associated with the odd part of the time-domain response



Causality Violations



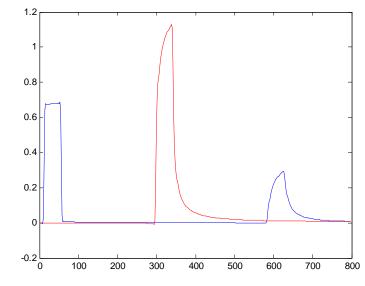
NON-CAUSAL

$$Z(f) = R_o \sqrt{f} + jL\omega$$

Near (blue) and Far (red) end responses of lossy TL



$$Z(f) = R_o \sqrt{f} + jR_o \sqrt{f} + jL\omega$$



Causality Principle

Consider a function h(t)

$$h(t) = 0, \quad t < 0$$

Every function can be considered as the sum of an even function and an odd function

$$h(t) = h_e(t) + h_o(t)$$

$$h_e(t) = \frac{1}{2} [h(t) + h(-t)]$$
 Even function

$$h_o(t) = \frac{1}{2} [h(t) - h(-t)]$$
 Odd function

$$h_o(t) = \begin{cases} h_e(t), & t > 0 \\ -h_e(t), & t < 0 \end{cases}$$

$$h_o(t) = \operatorname{sgn}(t)h_e(t)$$



Hilbert Transform

$$h(t) = h_e(t) + \operatorname{sgn}(t)h_e(t)$$

In frequency domain this becomes

$$H(f) = H_e(f) + \frac{1}{j\pi f} * H_e(f)$$

$$H(f) = H_e(f) - j\hat{H}_e(f)$$

→Imaginary part of transfer function is related to the real part through the Hilbert transform

 $\hat{H}_e(f)$ is the Hilbert transform of $H_e(f)$

$$\hat{x}(t) = x(t) * \frac{1}{\pi t} = \frac{1}{\pi} \int_{-\infty}^{+\infty} \frac{x(\tau)}{t - \tau} d\tau$$



Discrete Hilbert Transform

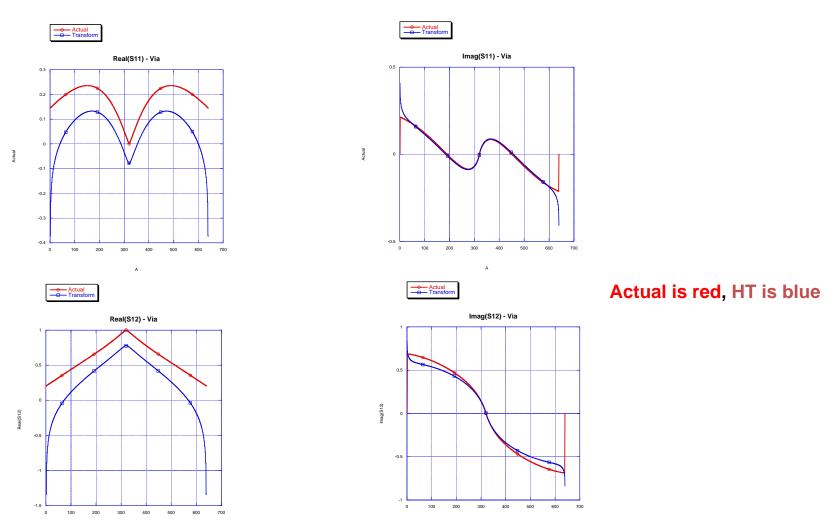
- → Imaginary part of transfer function can be recovered from the real part through the Hilbert transform
 - →If frequency-domain data is discrete, use discrete Hilbert Transform (DHT)*

$$H(f_n) = \hat{f}_k = \begin{cases} \frac{2}{\pi} \sum_{n \text{ odd}} \frac{f_n}{k - n}, & k \text{ even} \\ \frac{2}{\pi} \sum_{n \text{ even}} \frac{f_n}{k - n}, & k \text{ odd} \end{cases}$$

*S. C. Kak, "The Discrete Hilbert Transform", Proceedings of the IEEE, pp. 585-586, April 1970.



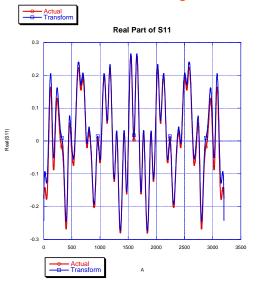
HT for Via: 1 MHz - 20 GHz

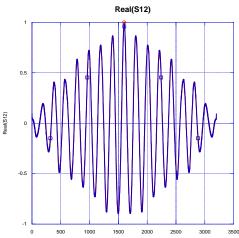


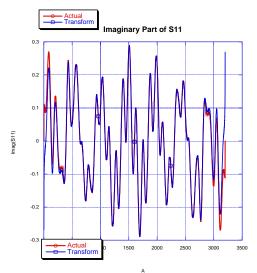
Observation: Poor agreement (because frequency range is limited)



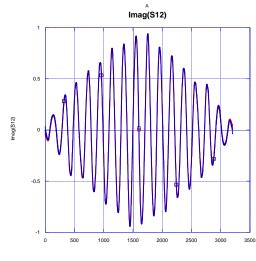
Example: 300 KHz - 6 GHz







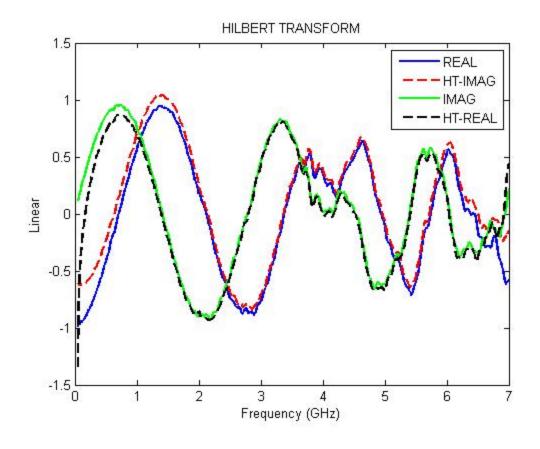




Observation: Good agreement

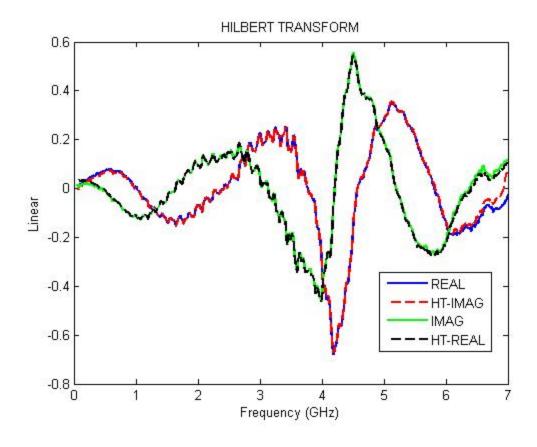


Microstrip Line S11



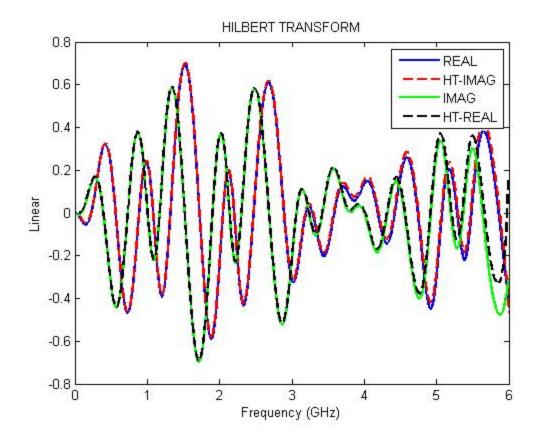


Microstrip Line S21



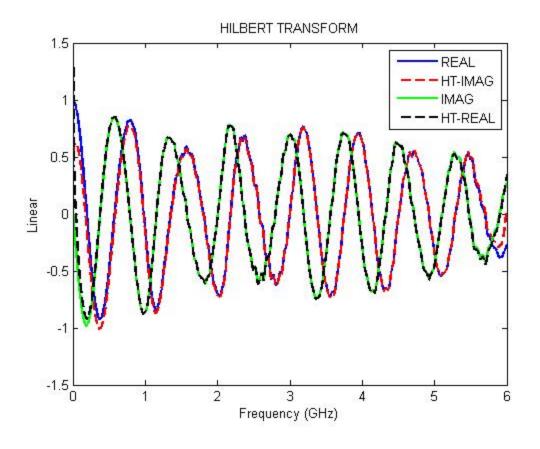


Discontinuity S11



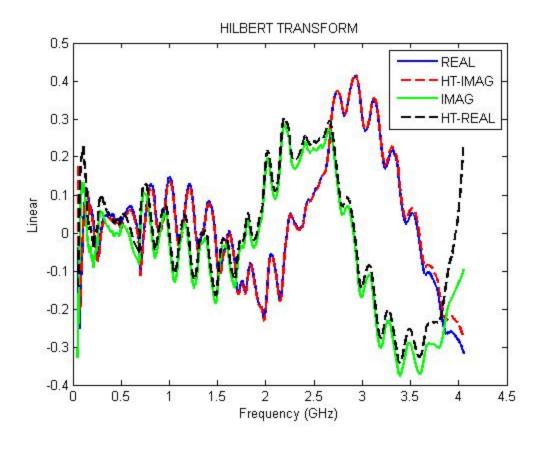


Discontinuity S21





Backplane S11





Backplane S21

